

bmcs course

Energy Games

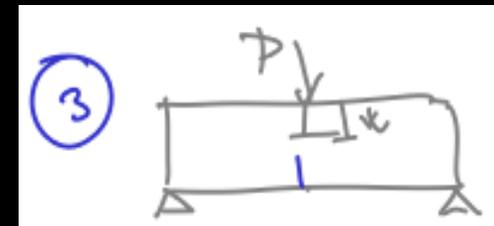
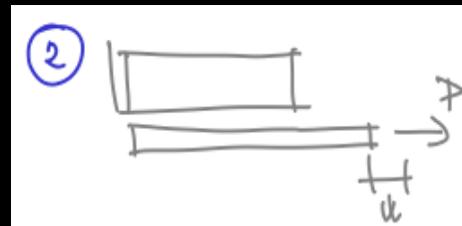
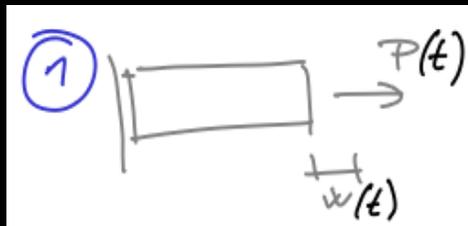
work supply, stored energy, energy dissipation

Rostislav Chudoba

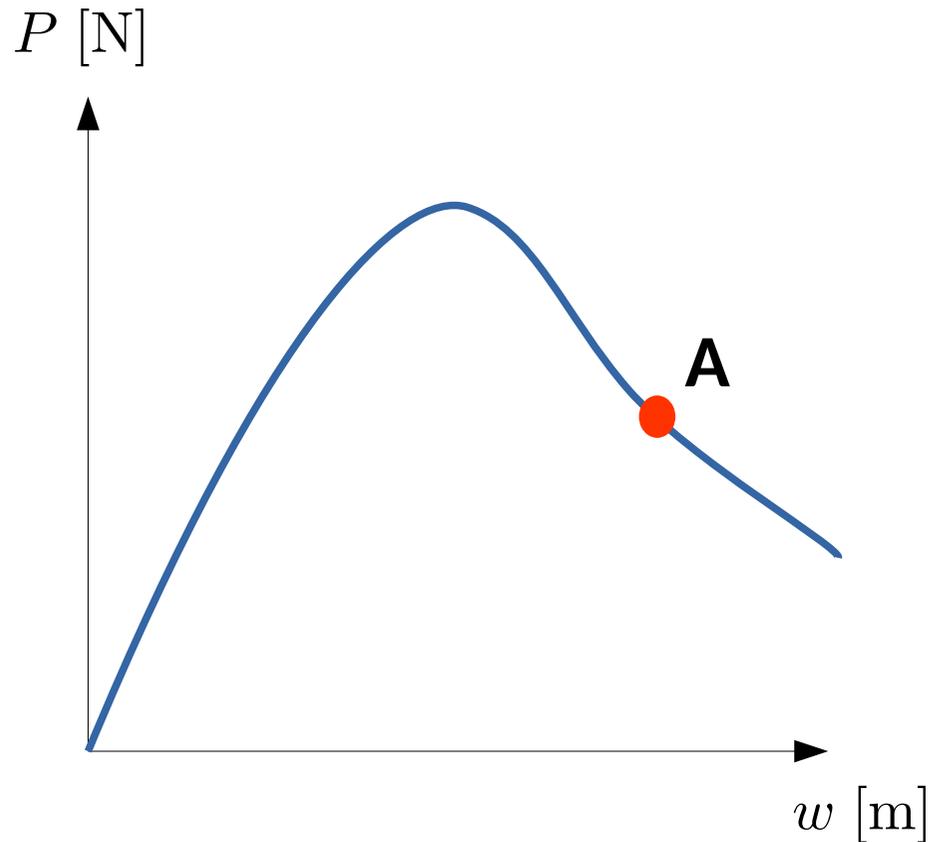
Abedulgader Baktheer

Institute of Structural Concrete

work supply

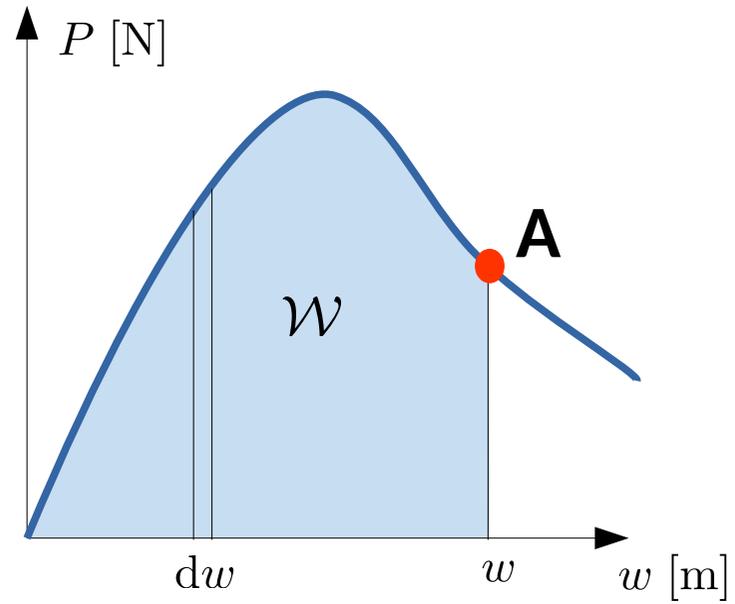
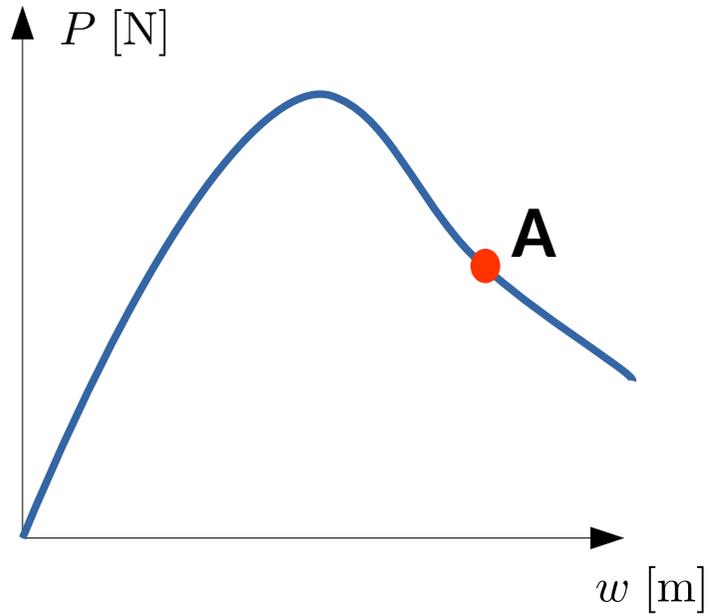


There is even more information hidden in the pull-out curve

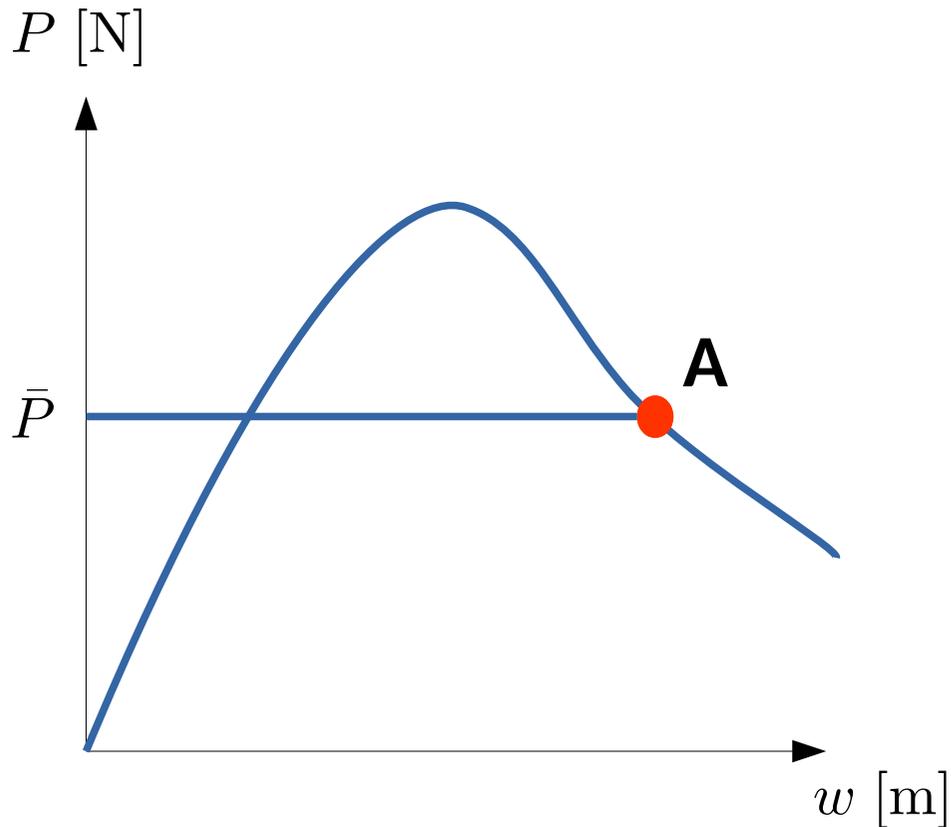


How much energy do we have to supply to reach the point A?

There is even more information hidden in the pull-out curve



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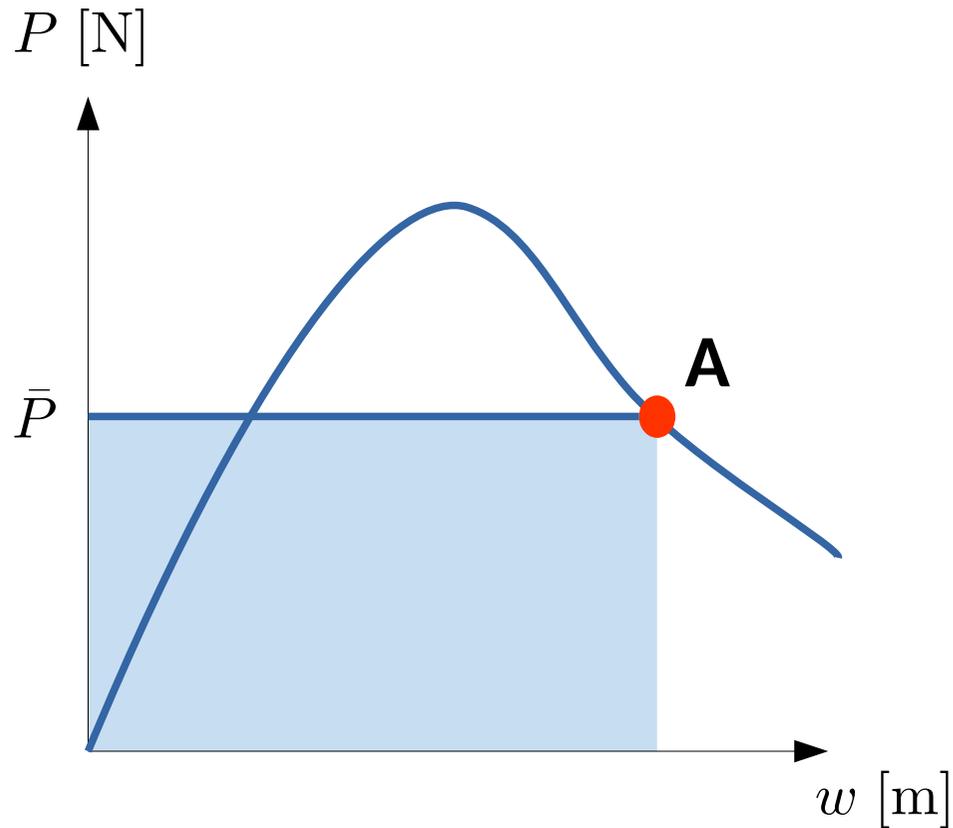


How much energy do we have to supply to reach the point A?

Recall the work definition:
assuming constant force \bar{P} [N]
the work needed to displace
an object to w [m] is

$$W = \bar{P}w \text{ [Nm]}$$

There is even more information hidden in the pull-out curve

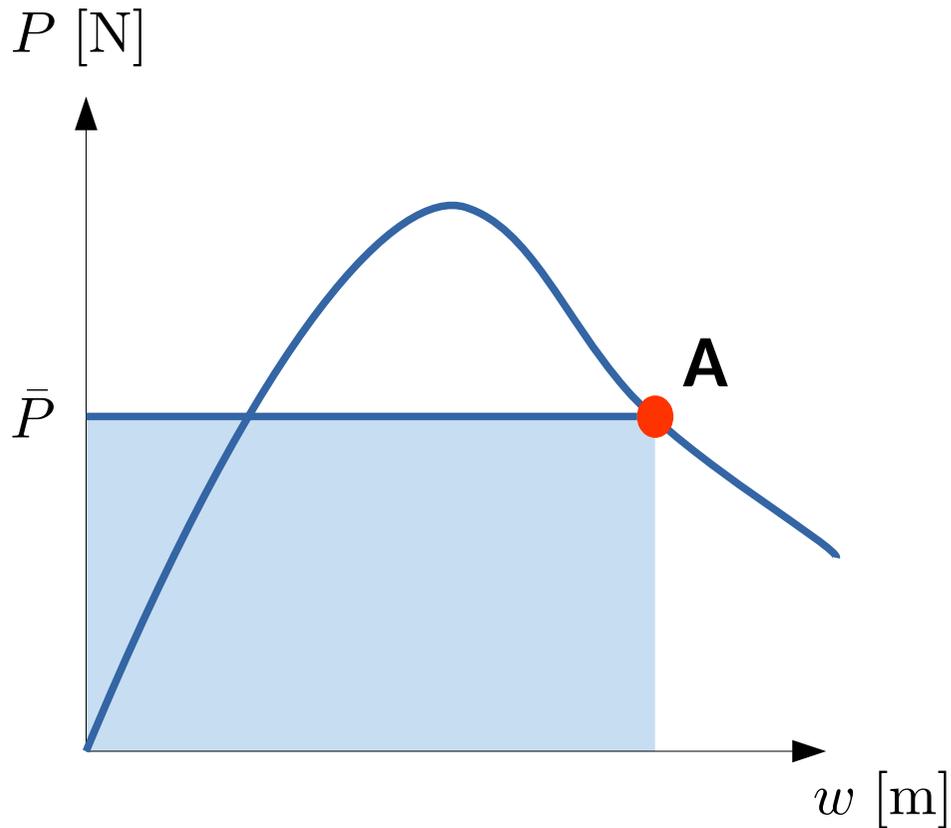


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Work supply



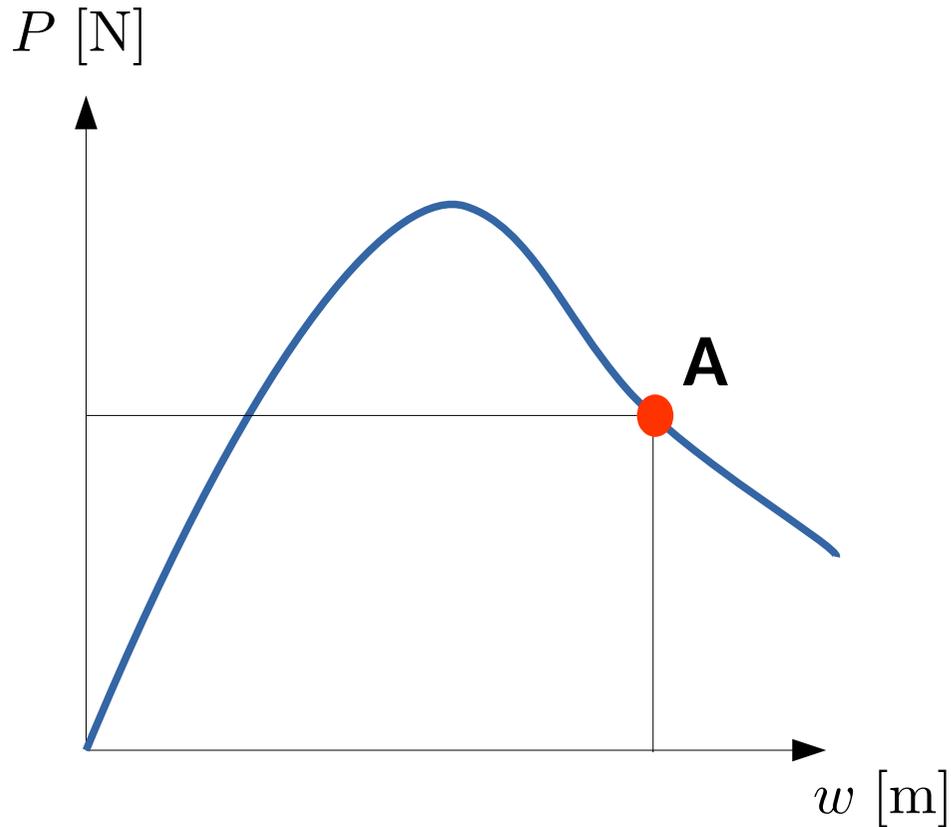
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BUT what if $P(w) \neq \text{constant}$

Work supply



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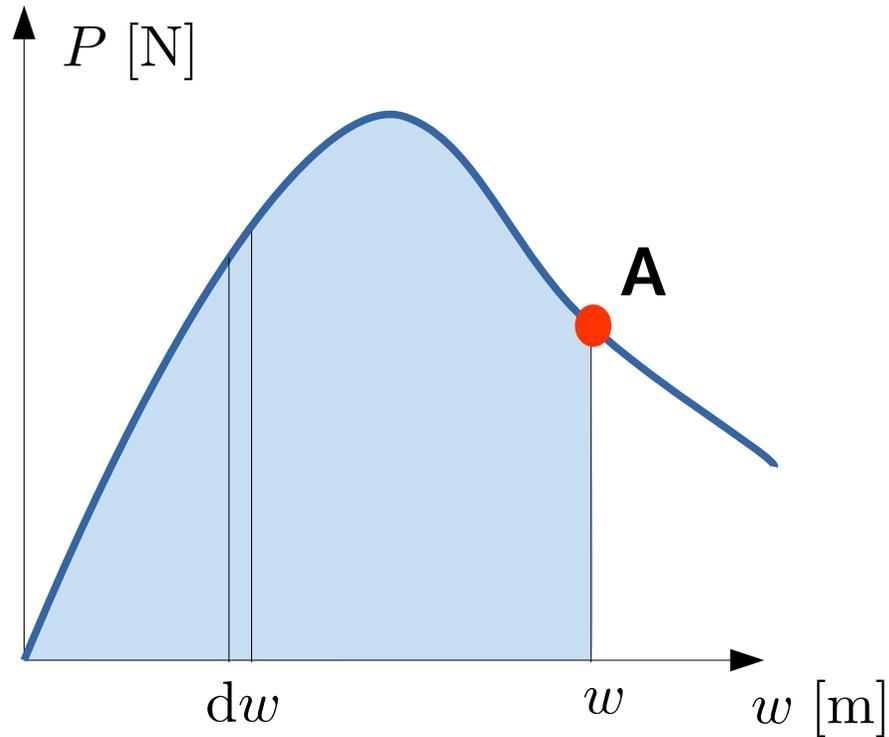
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BUT what if $P(w) \neq \text{constant}$

THEN $dW = P(w) dw$

Work supply



How much energy do we have to supply to reach the point A?

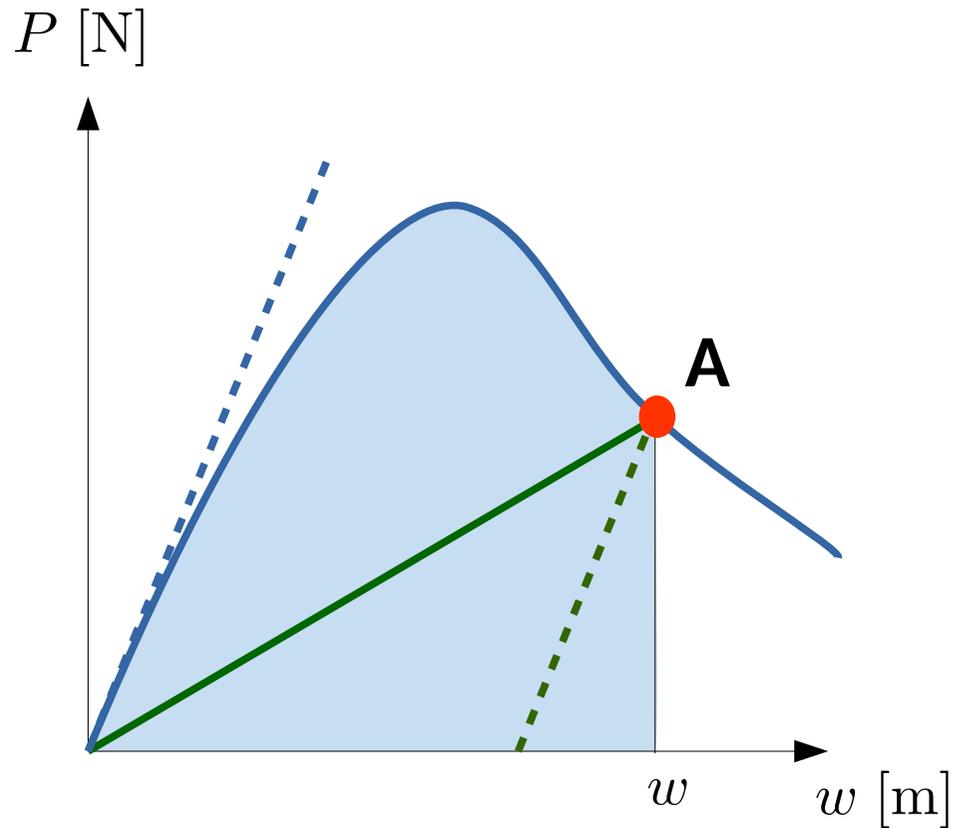
$$dW = P(w) dw$$

$$W = \int_0^w P(w) dw$$

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the battery – stored energy

Stored energy



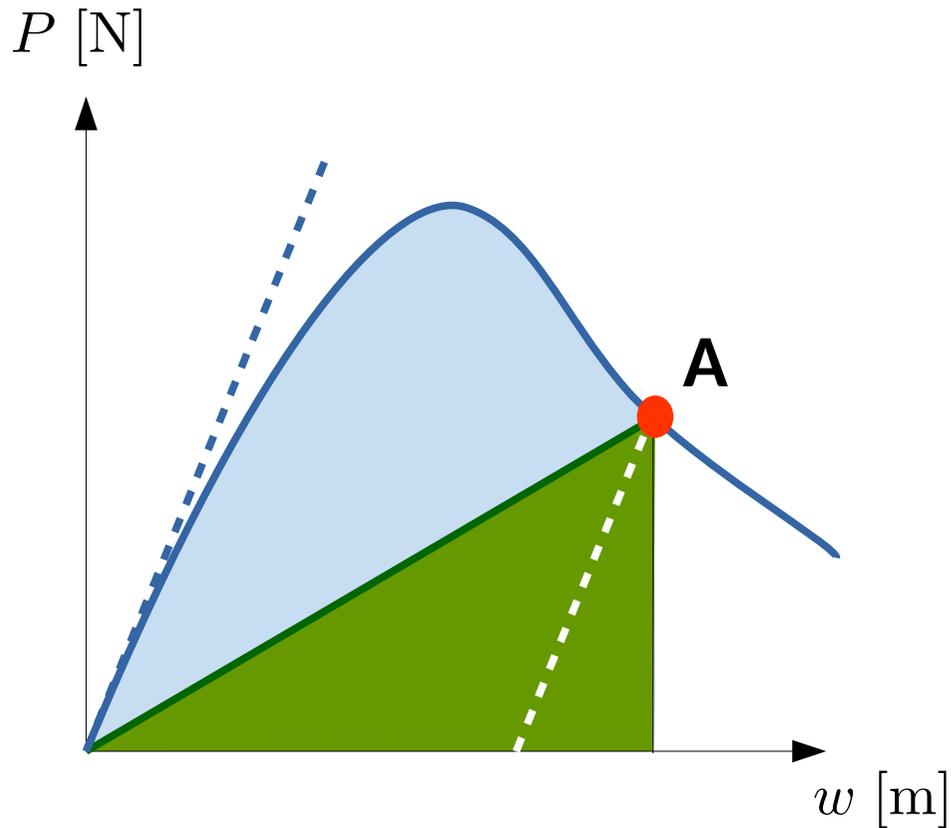
How much energy can be recovered by unloading?

It depends ...

Are you asking this for material behavior governed by damage or by plasticity?

$$W = \int_0^w P(w) dw$$

Stored energy



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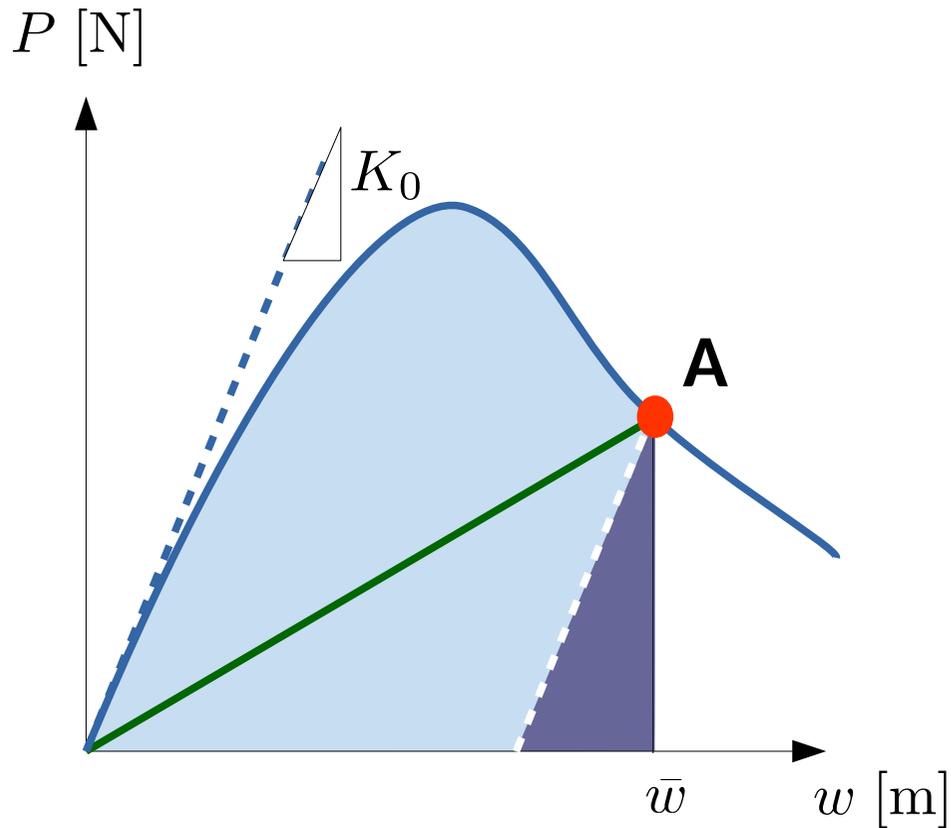
Are you asking this for material behavior governed by damage or by plasticity?

damage

$$U_w = \frac{1}{2} Pw$$

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} Pw$$

Stored energy



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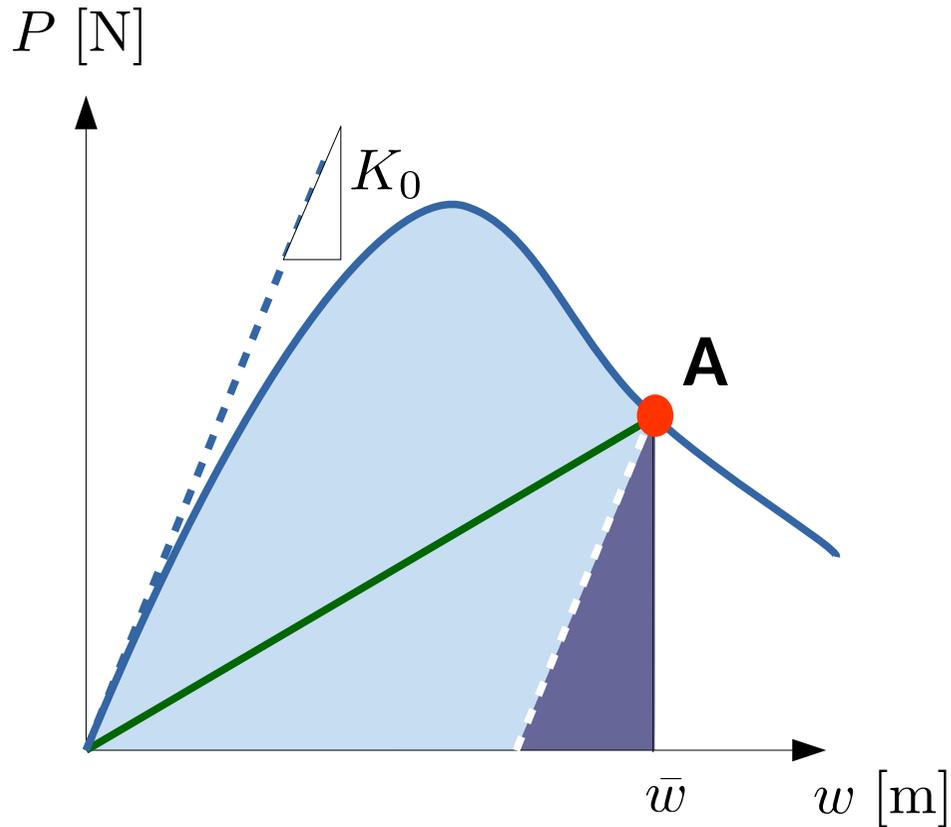
$$U_{\omega} = \frac{1}{2} P w$$

plasticity

$$U_{\pi} = \frac{1}{2} P \left(\frac{P}{K_0} \right)$$

$$W = \int_0^w P(w) dw \quad U_{\omega} = \frac{1}{2} P w$$

Stored energy



How much energy can be recovered by unloading?

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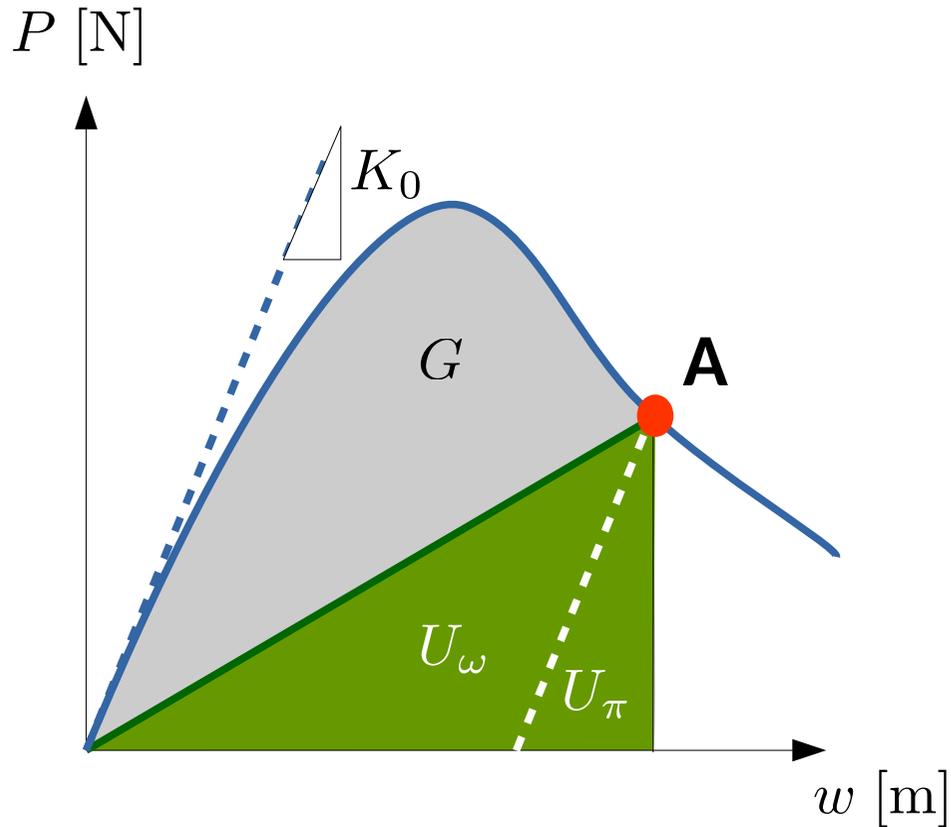
$$U_\omega = \frac{1}{2} P w$$

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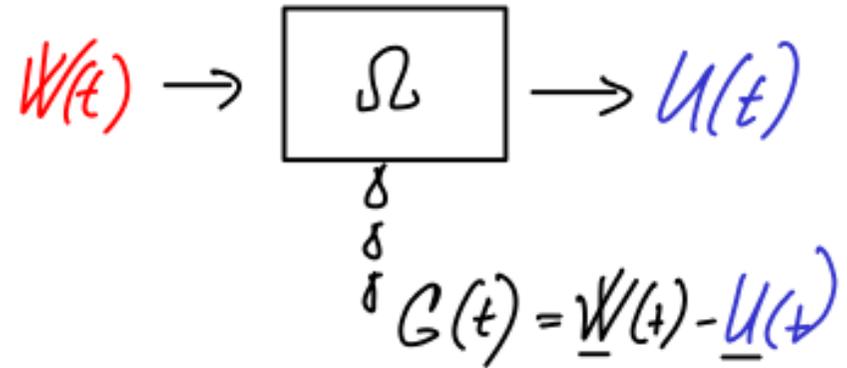
$$W = \int_0^w P(w) dw \quad U_\omega = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0}$$

the energy release

Dissipated energy



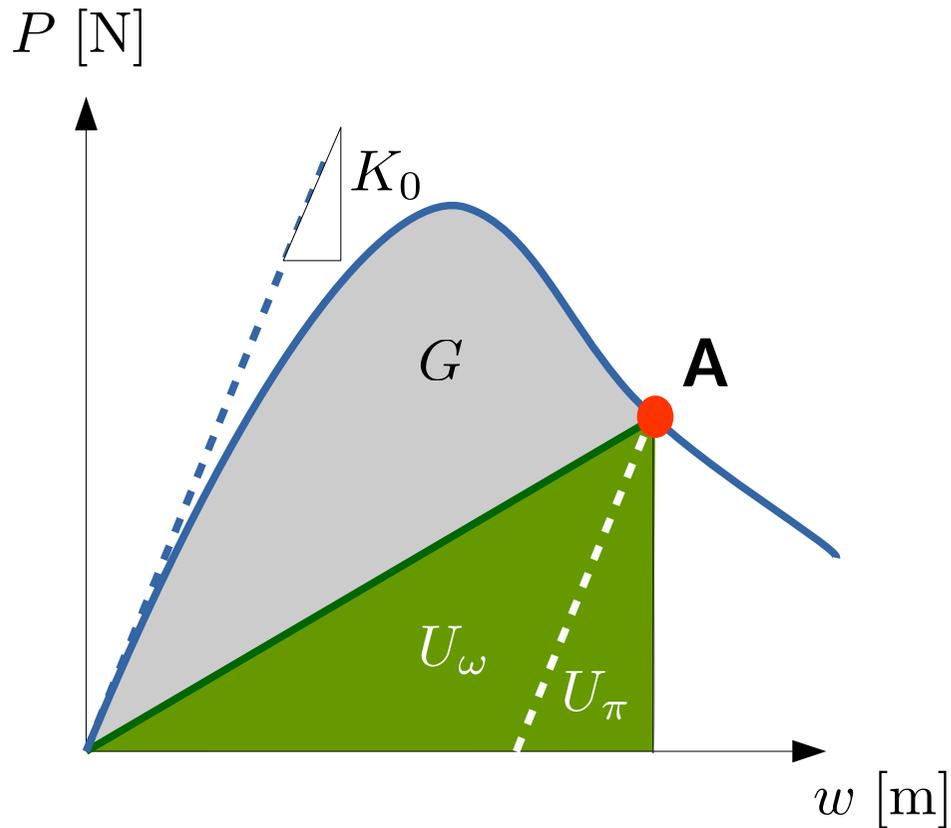
How big was the energy leak?



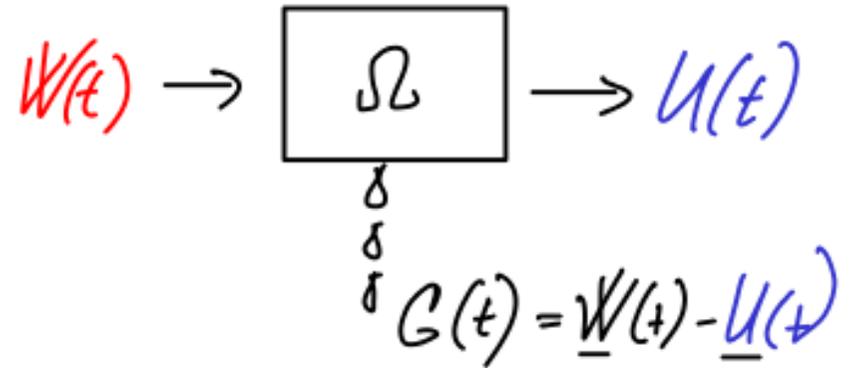
$$G = W - U = \int_0^w P(w) dw - U(w)$$

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Dissipated energy



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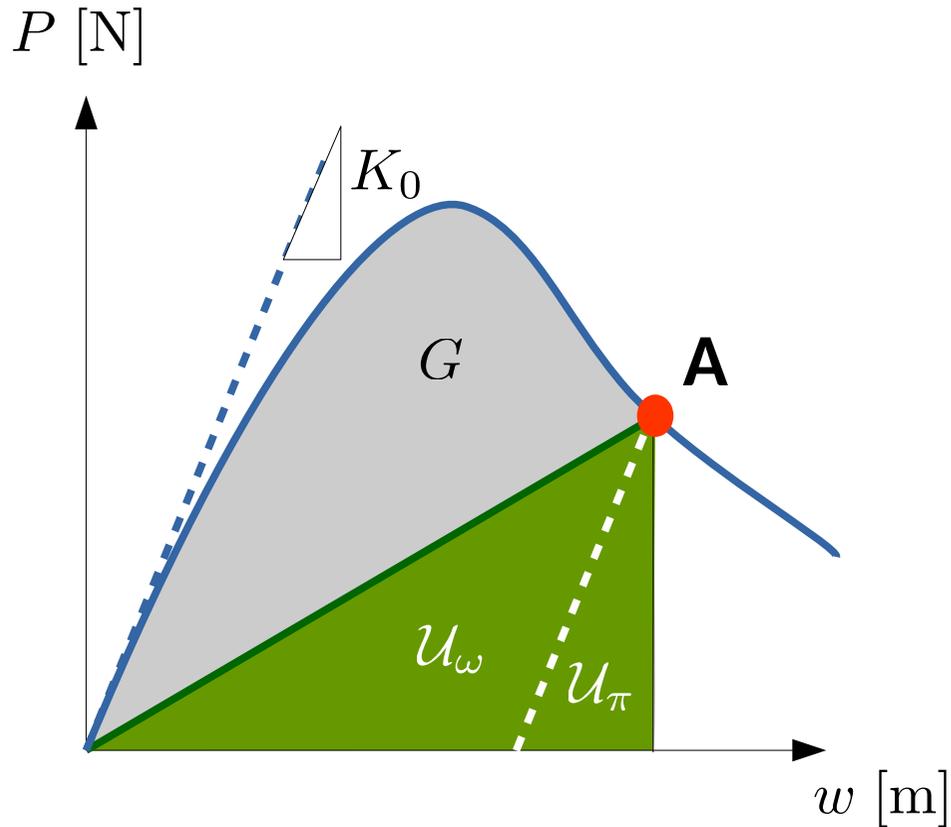


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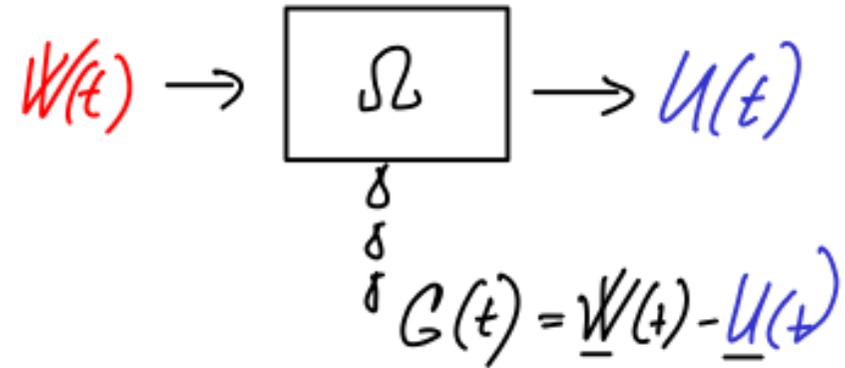
material behavior, boundary conditions, geometry

$$W = \int_0^w P(w) dw \quad U_\omega = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U$$

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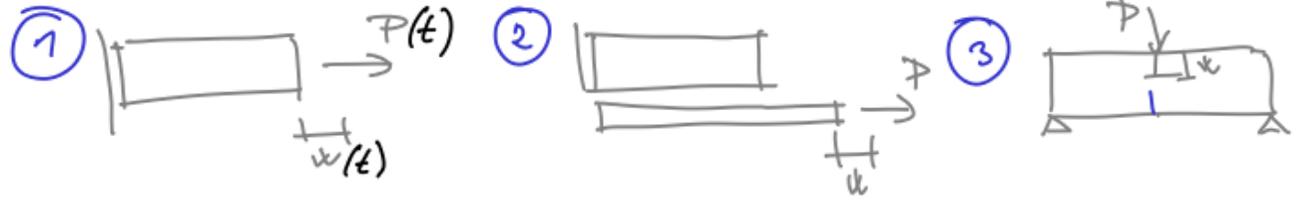
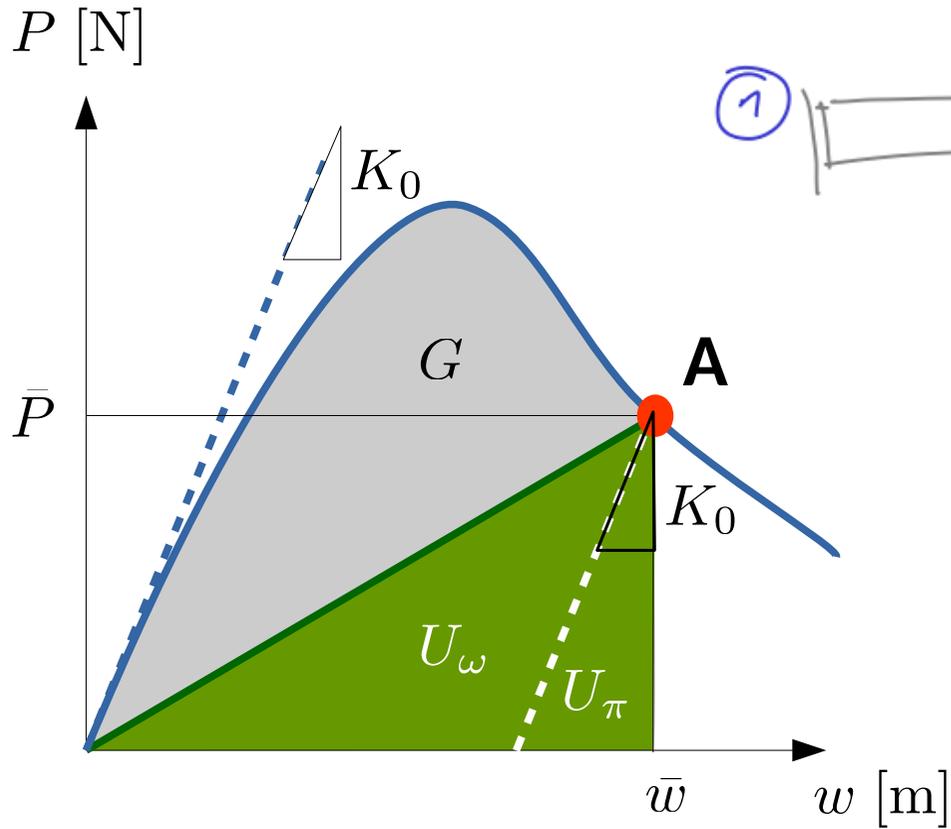


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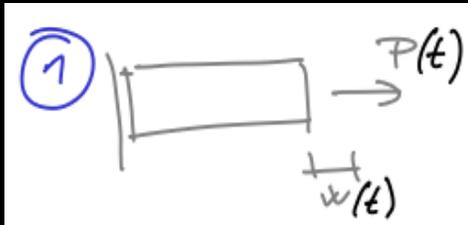


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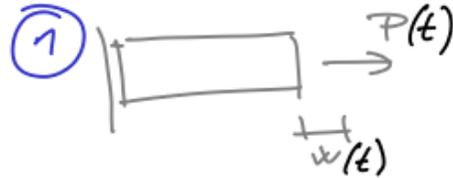
elastic bar



$$G = ?$$

Dissipated energy – elastic bar loaded in tension

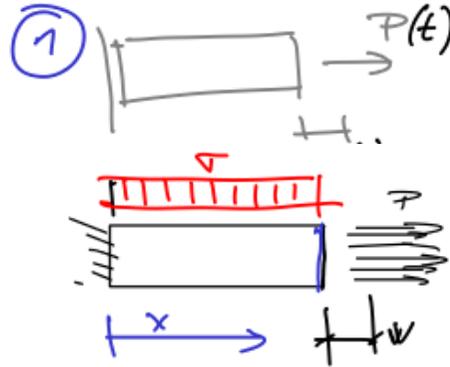
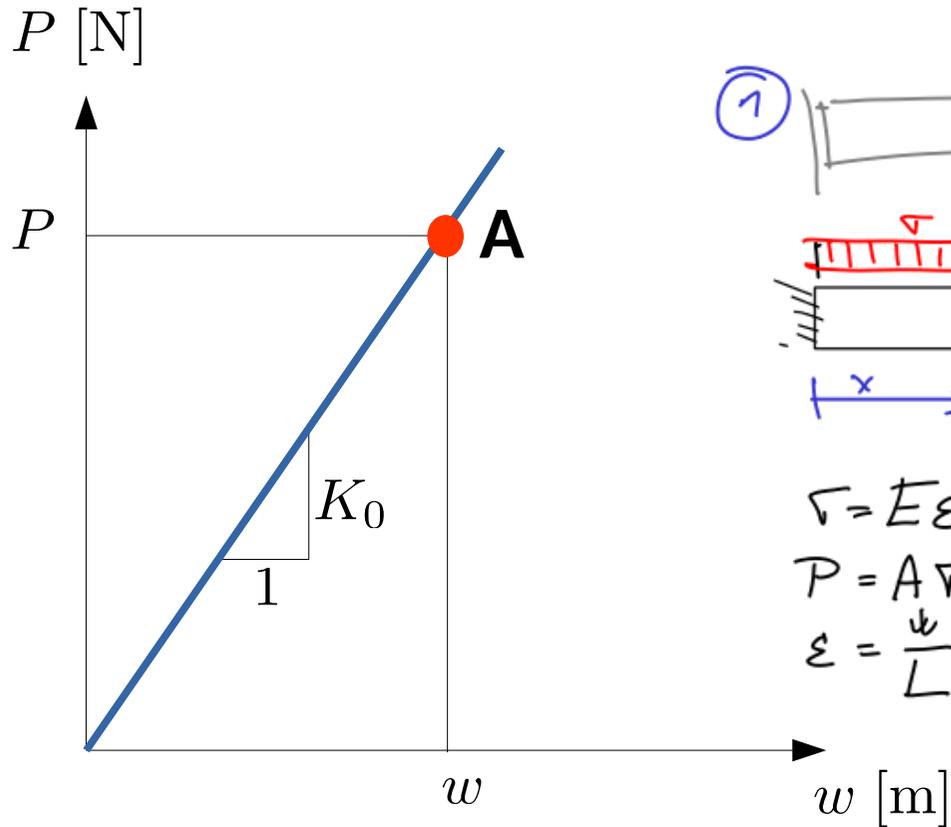
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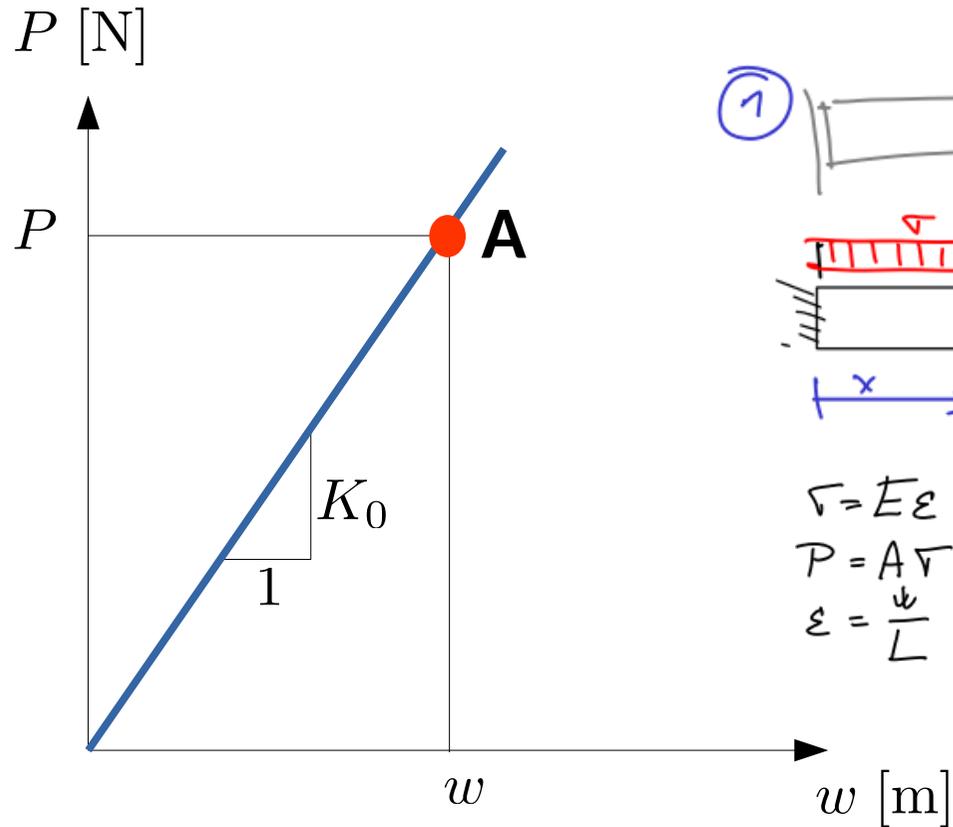
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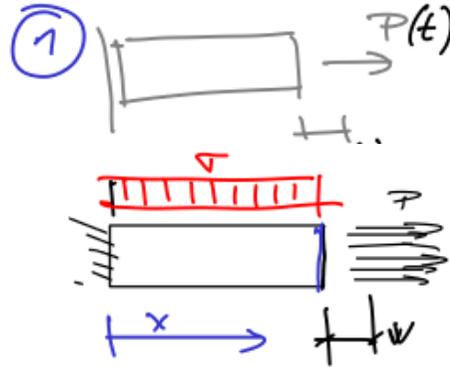
$\sigma = E \epsilon$ - const. law
 $P = A \sigma$ - equilibrium
 $\epsilon = \frac{w}{L}$ - kinematics

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U$$

Dissipated energy – elastic bar loaded in tension



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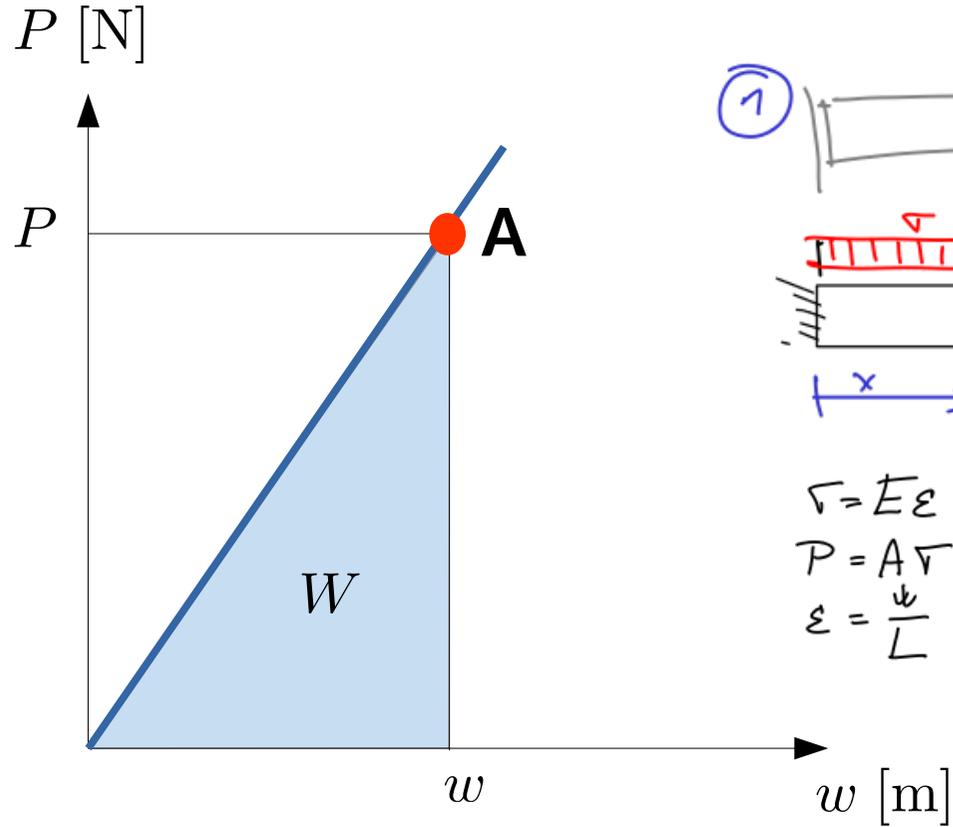
$$W = \int_0^w \frac{EA}{L} w dw = \frac{EA}{2L} w^2$$

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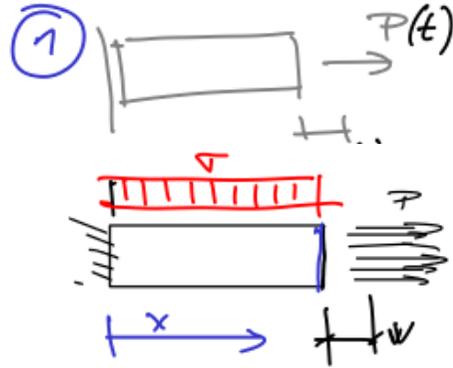
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Dissipated energy – elastic bar loaded in tension



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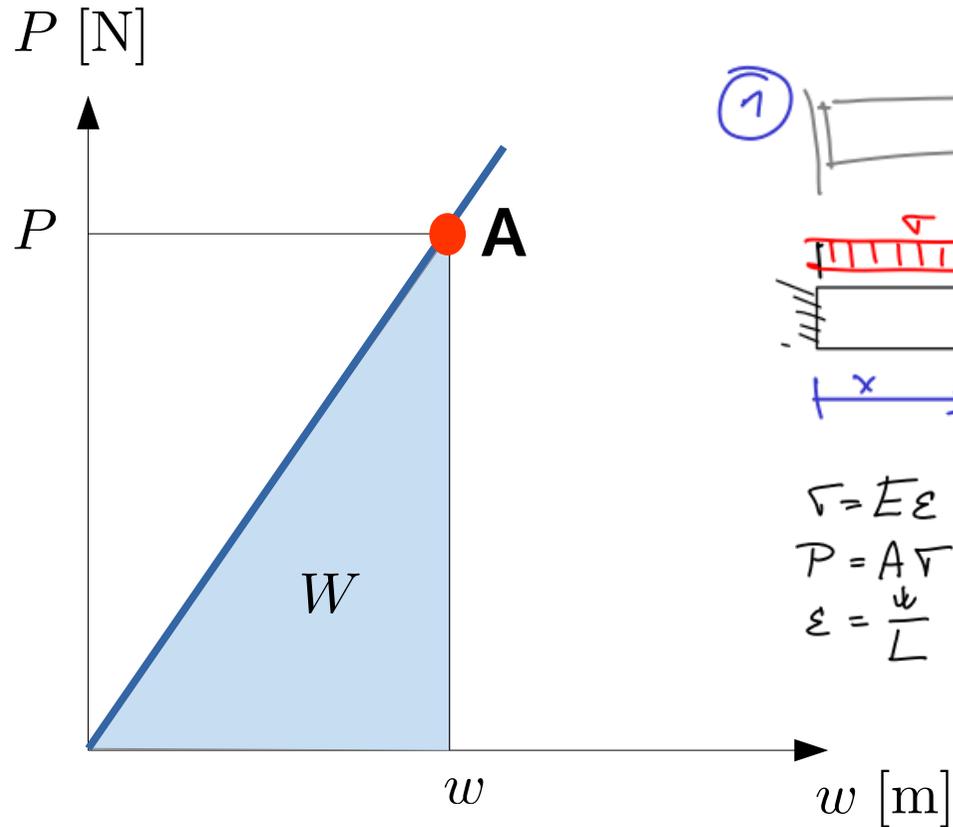
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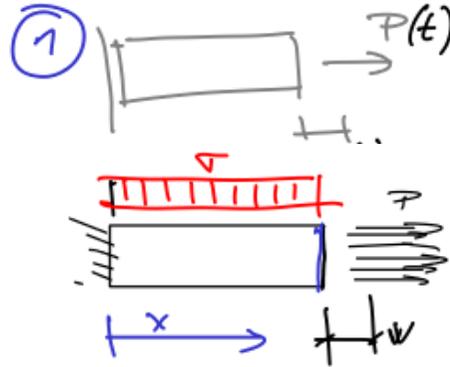
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Dissipated energy – elastic bar loaded in tension



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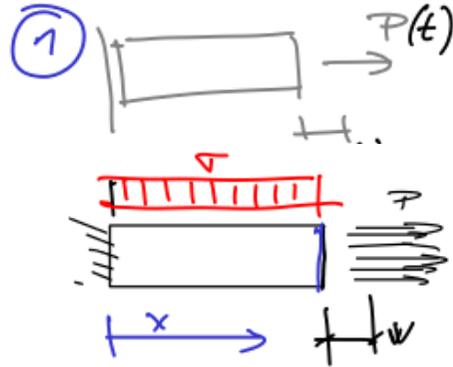
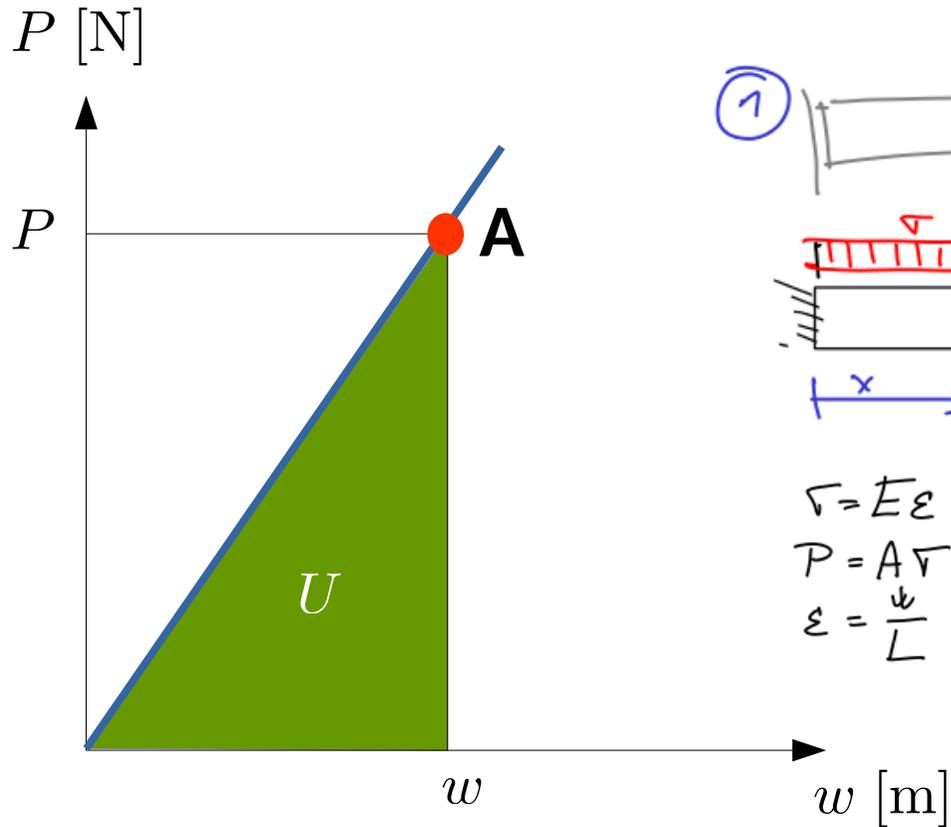
$$U = \frac{1}{2} \cdot \frac{EA}{L} w \cdot w$$

- $\sigma = E \varepsilon$ - const. law
- $P = A \sigma$ - equilibrium
- $\varepsilon = \frac{w}{L}$ - kinematics

$$P = \frac{EA}{L} w$$

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U$$

Dissipated energy – elastic bar loaded in tension



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$$W = \int_0^w \frac{EA}{L} w dw = \frac{EA}{2L} w^2$$

$$U = \frac{EA}{2L} w^2$$

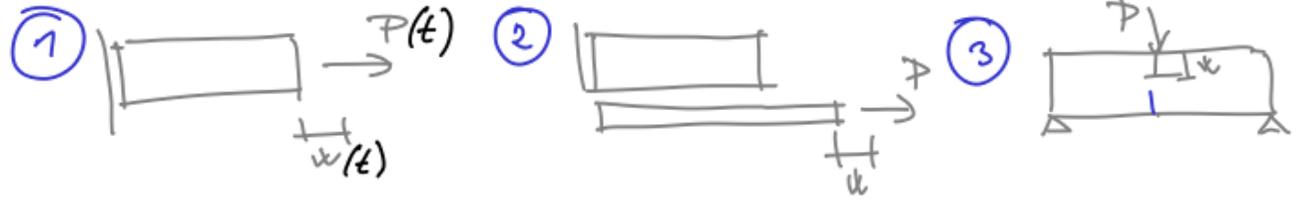
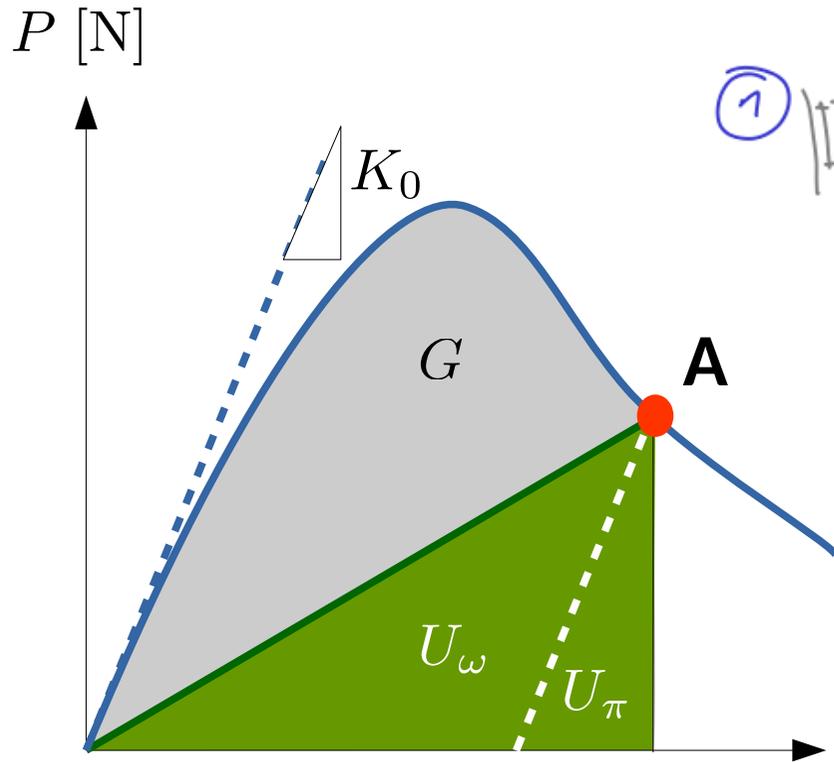
$$G = W - U = 0$$

$$P = \frac{EA}{L} w$$

NO DISSIPATION

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U$$

Dissipated energy – pull-out from rigid matrix

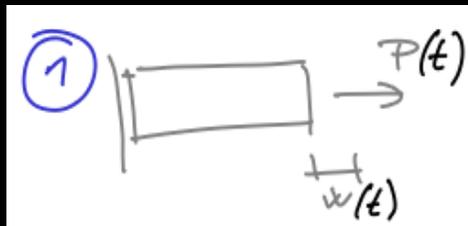


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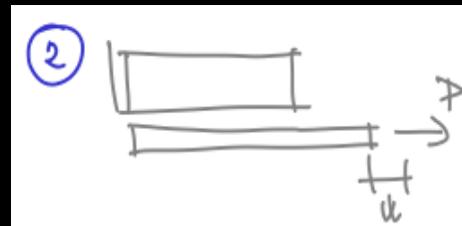
material behavior, boundary conditions, geometry

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elastic bar and frictional interface



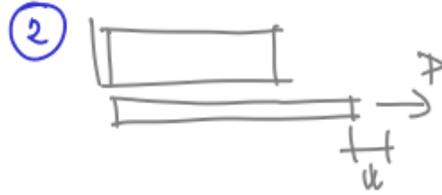
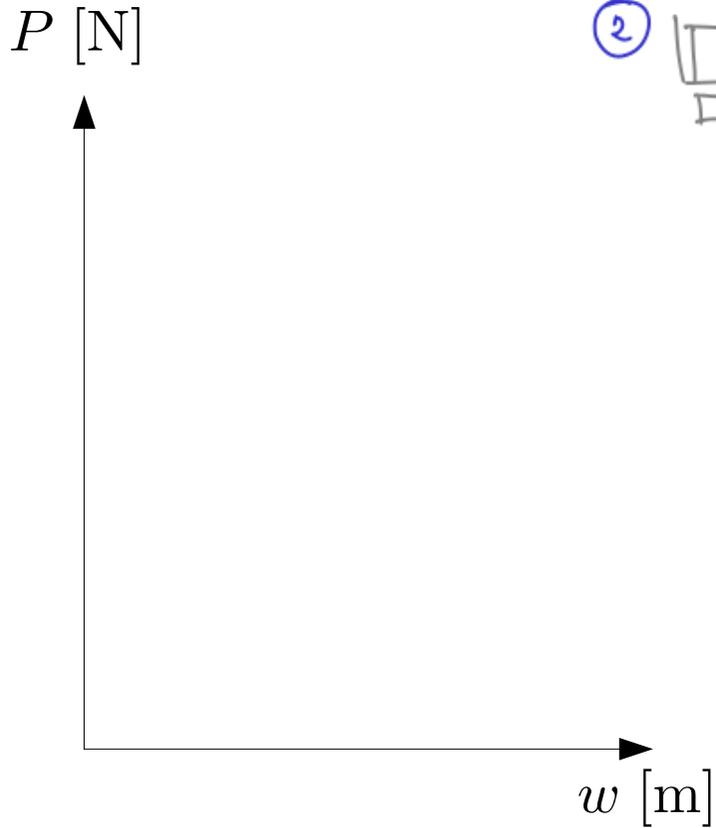
$$G = 0$$



$$G = ?$$

Dissipated energy – pull-out from rigid matrix

$$G = W - U = \int_0^w P(w) dw - U(w)$$



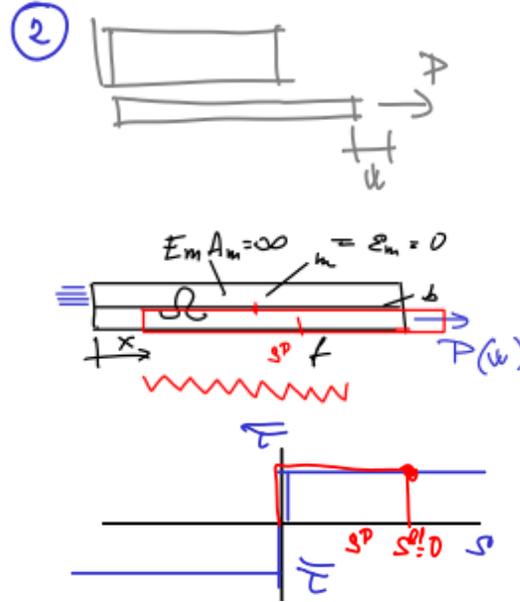
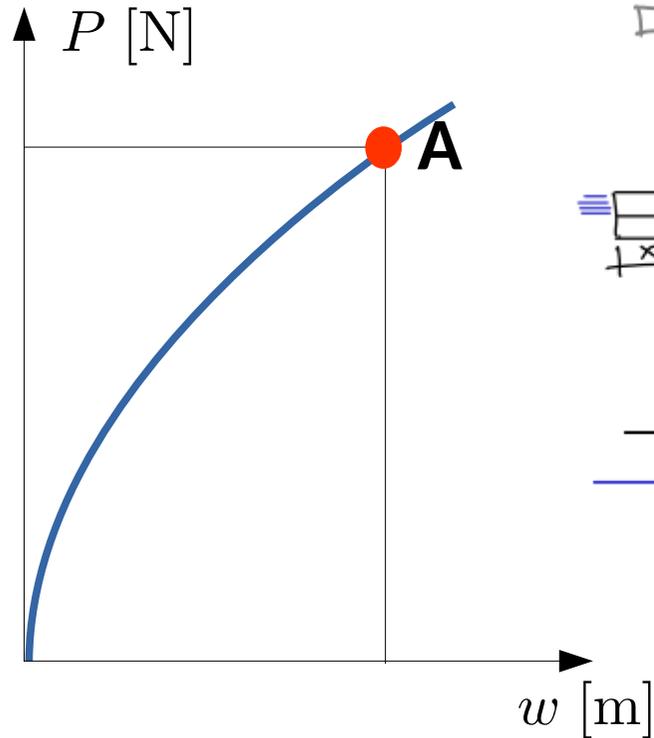
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Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

[see Tour 2]

$$G = W - U = \int_0^w P(w) dw - U(w)$$

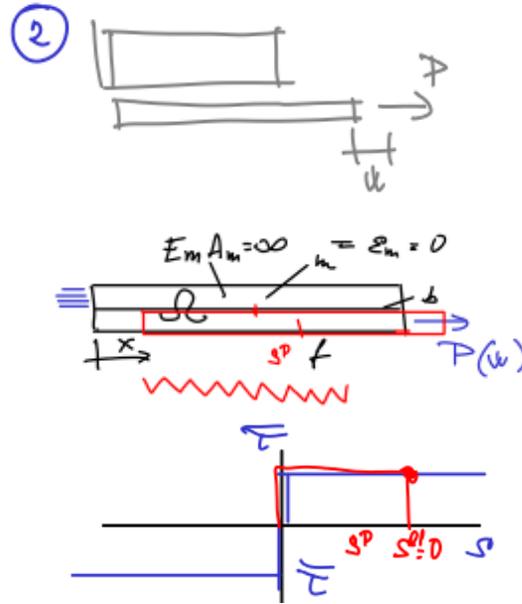
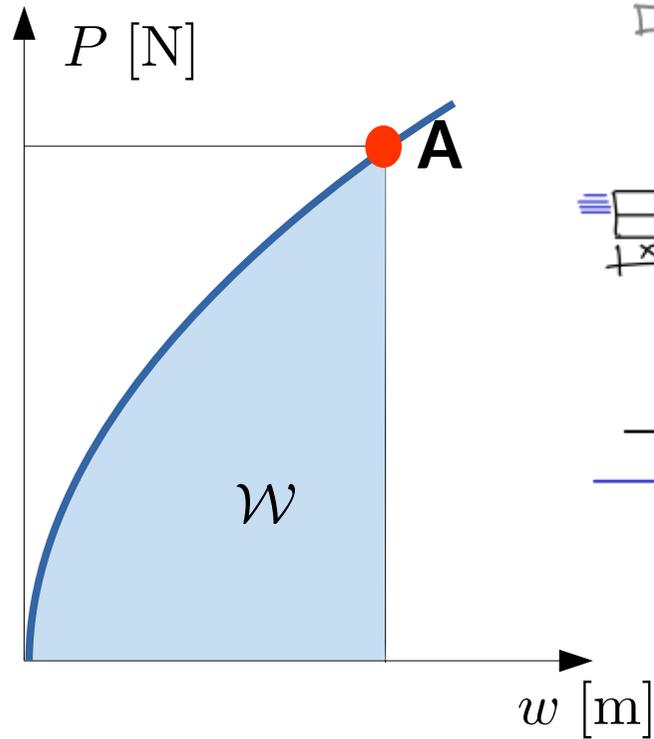


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Dissipated energy – pull-out from rigid matrix

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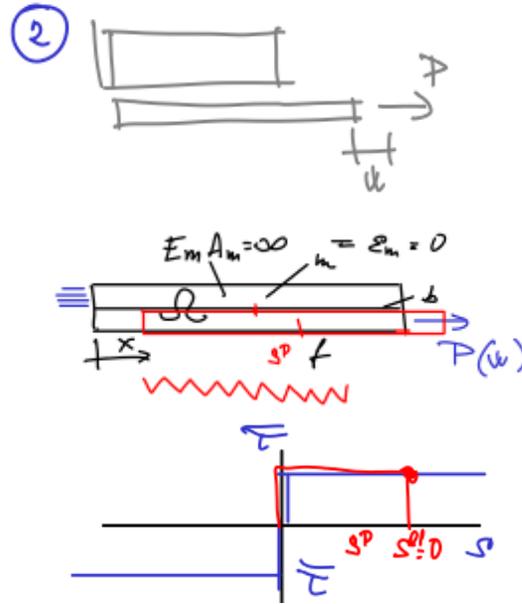
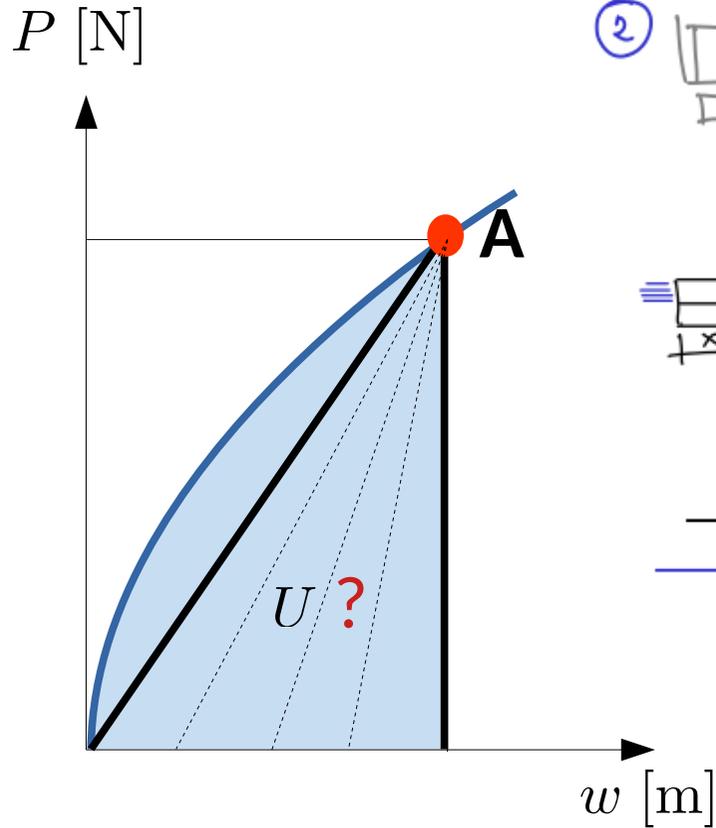
$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

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Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = ?$$

How much energy was stored?

How would the pull-out test unload?

Maybe along the initial stiffness?

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

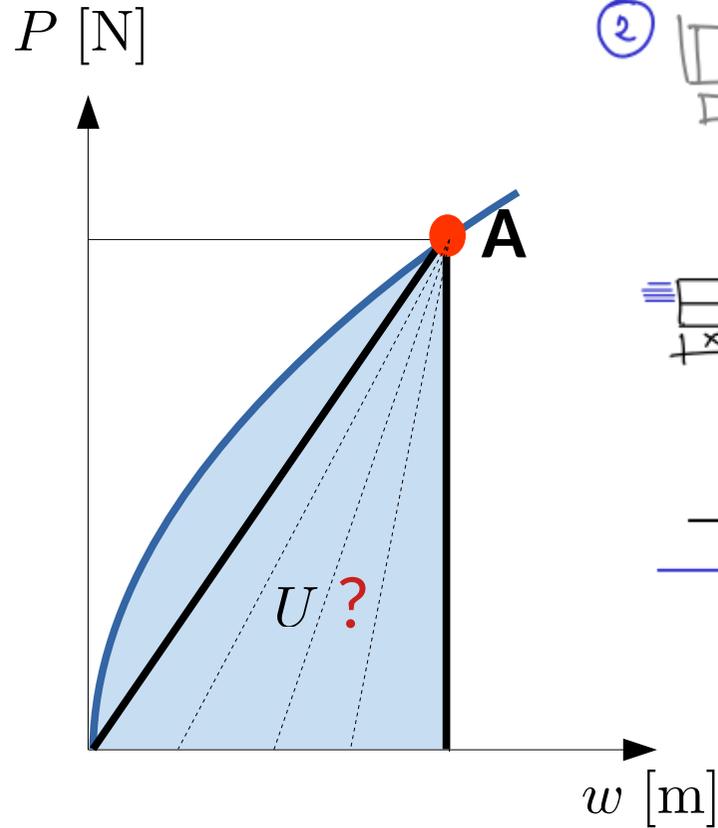
$$U_\pi = \frac{P^2}{2K_0}$$

$$G = W - U$$

$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$



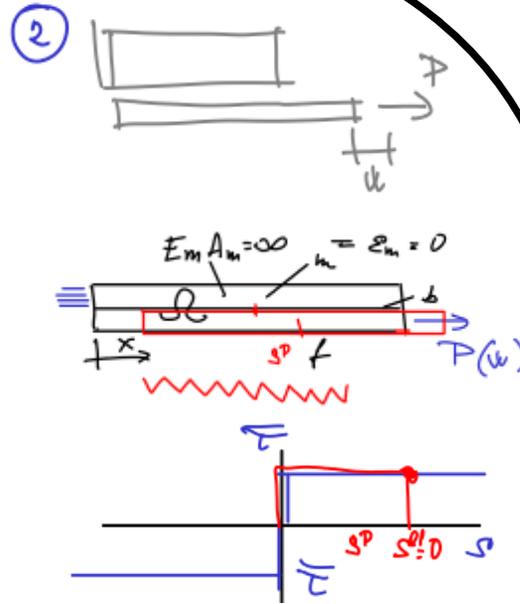
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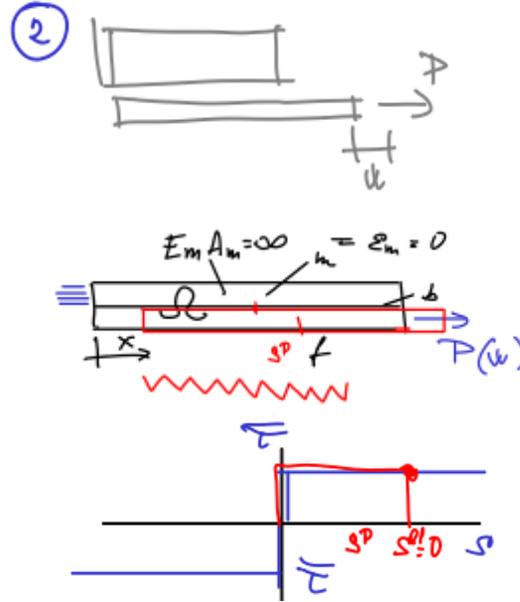
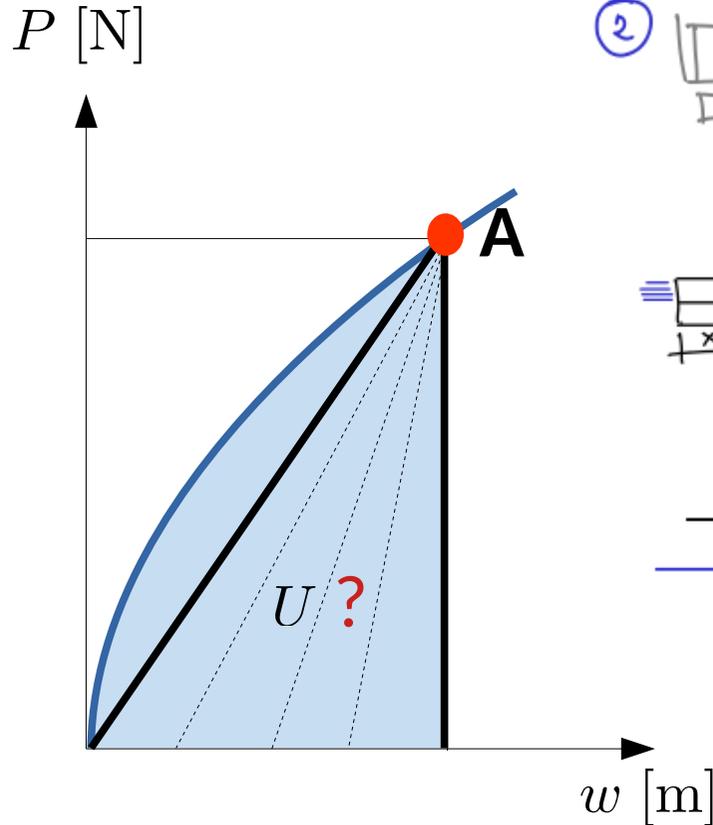
$$K_0 = \left. \frac{\partial P}{\partial w} \right|_{w=0} = \left. \frac{\sqrt{E_f A_f p \bar{\tau}}}{2\sqrt{w}} \right|_0 = \infty$$

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U \quad W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = ?$$

How much energy was stored?

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$$K_0 = \left. \frac{\partial P}{\partial w} \right|_{w=0} = \left. \frac{\sqrt{E_f A_f p \bar{\tau}}}{2\sqrt{w}} \right|_0 = \infty$$

But then - we would ignore the deformation of the pulled-out bar!
How much energy does it store?

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

$$U_\pi = \frac{P^2}{2K_0}$$

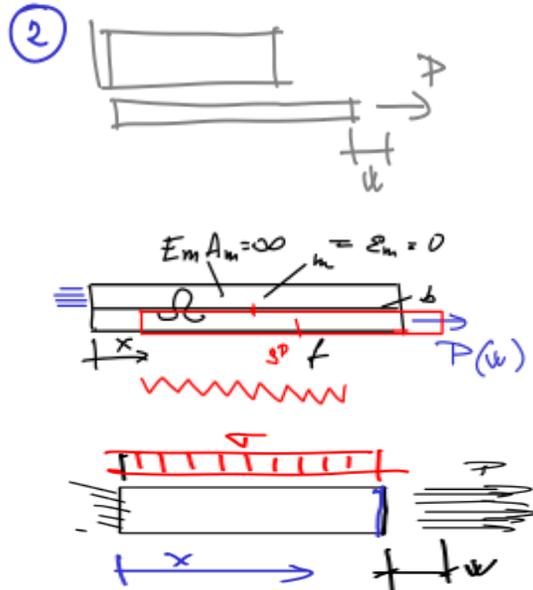
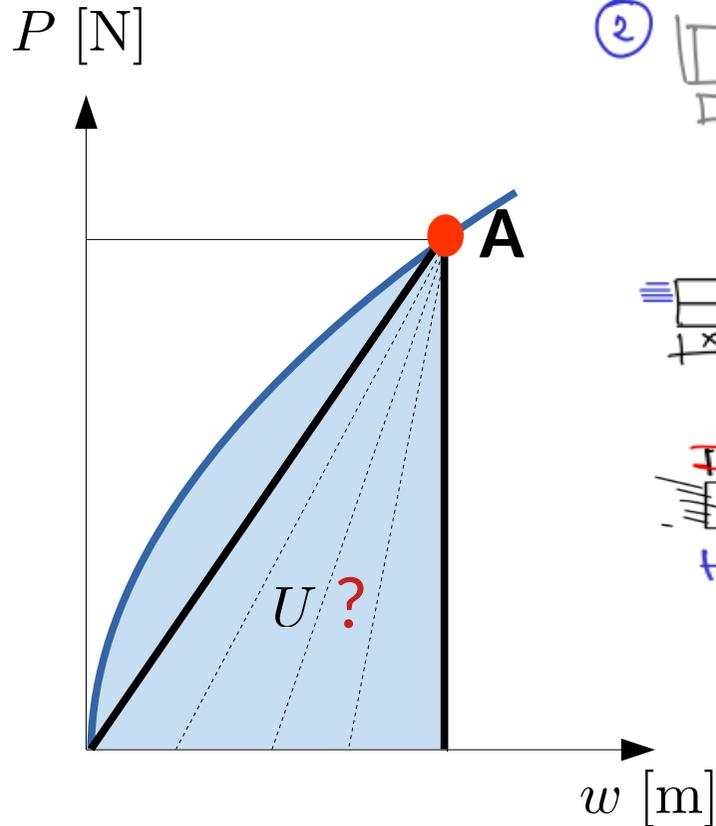
$$G = W - U$$

$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = ?$$

How much energy was stored?

How would the pull-out test unload?

Should we unload to the origin then?

Can we reuse the stored energy derived before for a tensile bar?

$$U = \frac{E_f A_f}{2L} w^2$$

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

$$U_\pi = \frac{P^2}{2K_0}$$

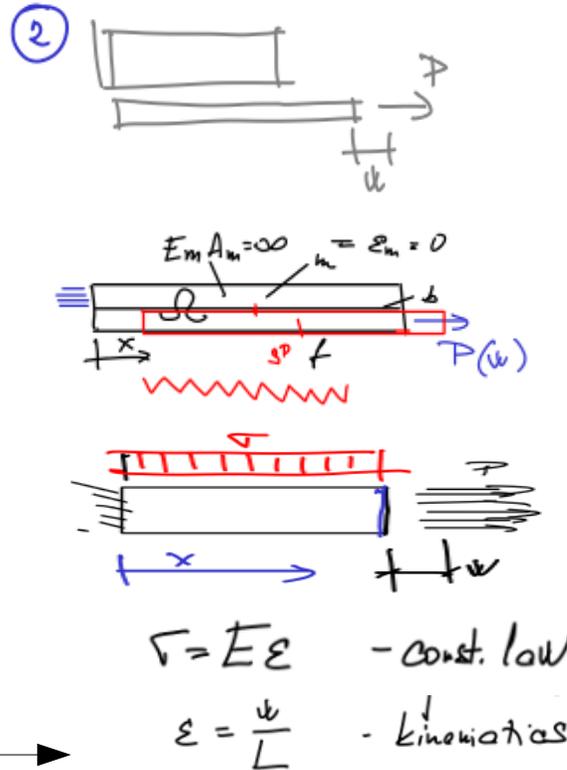
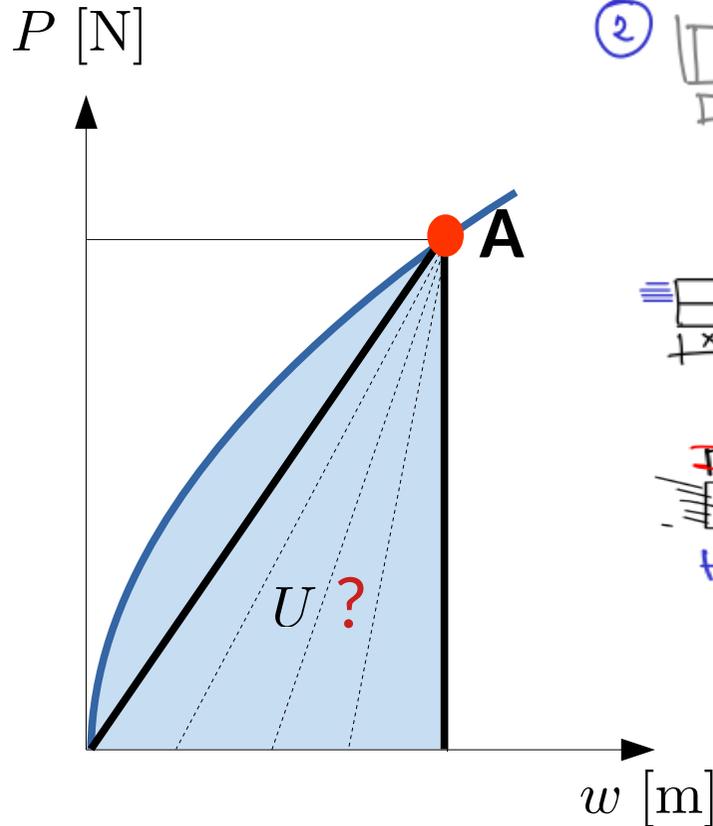
$$G = W - U$$

$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = ?$$

How much energy was stored?

How would the pull-out test unload?

Should we unload to the origin then?

Can we reuse the stored energy derived before for a tensile bar?

$$U = \frac{E_f A_f}{2L} w^2$$

NO - as it considered constant strain and stress along the bar

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

$$U_\pi = \frac{P^2}{2K_0}$$

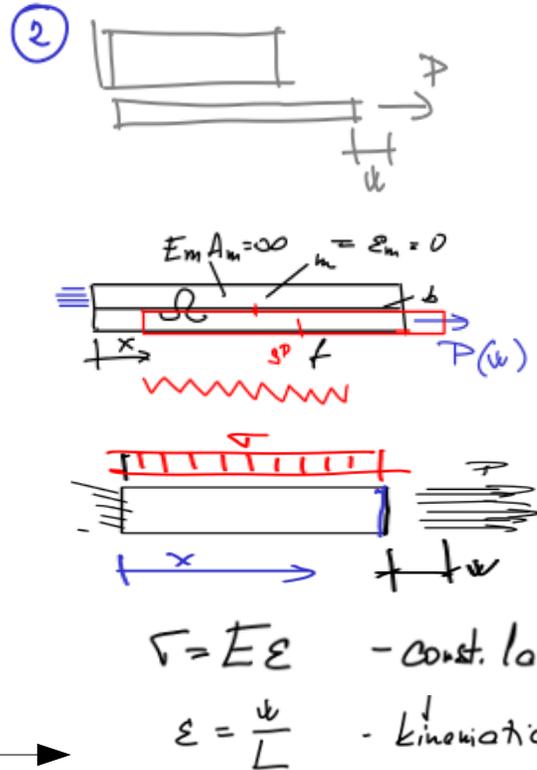
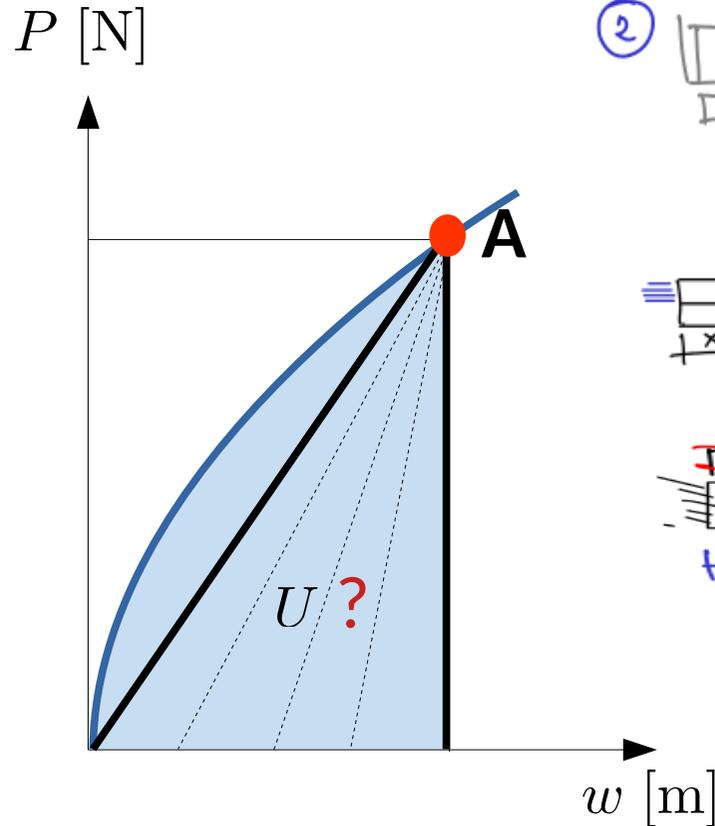
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Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = ?$$

How much energy was stored?

How would the pull-out test unload?

Solution: In case of elastic bar we actually evaluated an integral over energy stored in material points

$$U = \int_{\Omega} \sigma_{el}(x) \epsilon_{el}(x) dx$$

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

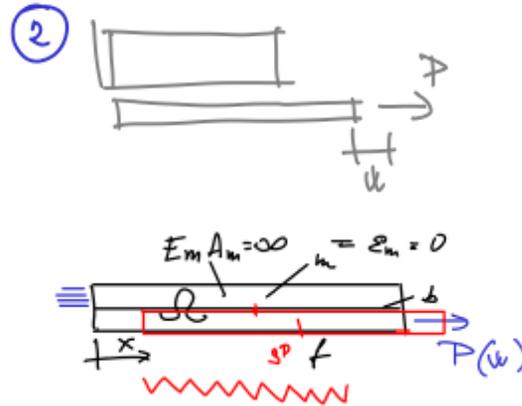
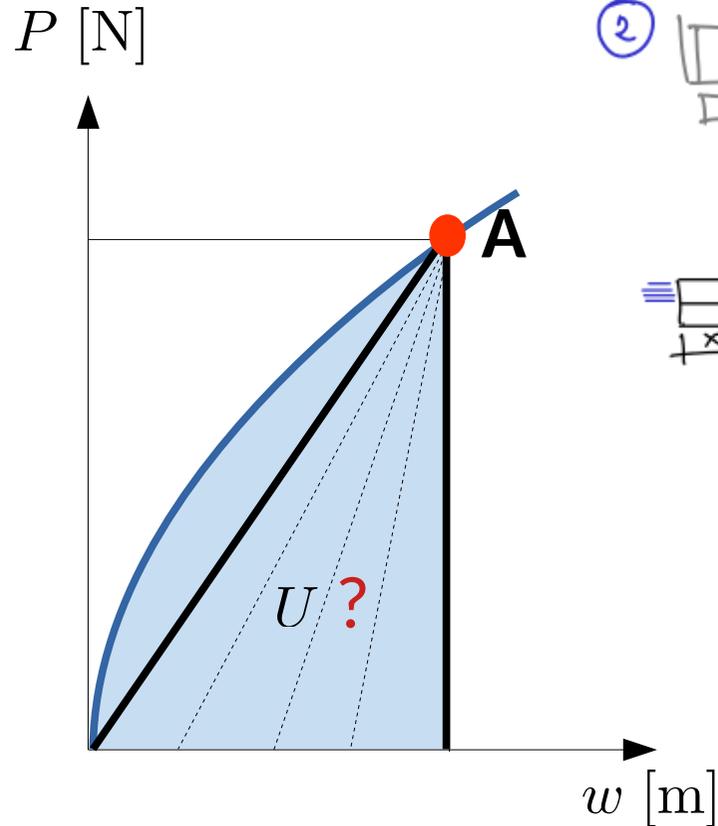
$$U_{\pi} = \frac{P^2}{2K_0}$$

$$G = W - U$$

$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$



$$G = W - U = \int_0^w P(w) dw - U(w)$$

$$U(w) = \int_{\Omega} \sigma_{el}(x) \varepsilon_{el}(x) dx$$

We already know these two fields for any value of control pull-out displacement

They were derived in Tour 2:

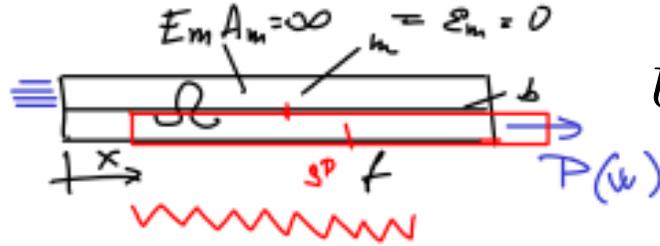
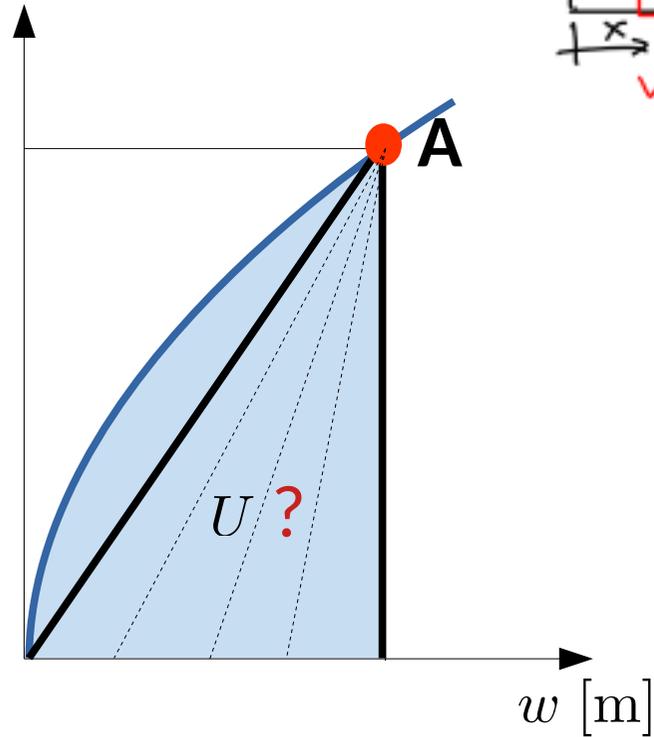
$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_{\pi} = \frac{P^2}{2K_0} \quad G = W - U \quad W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$

P [N]



$$U(w) = \int_{\Omega} \sigma_{el}(x) \varepsilon_{el}(x) dx$$

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

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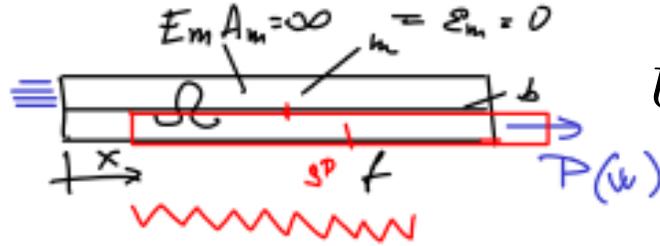
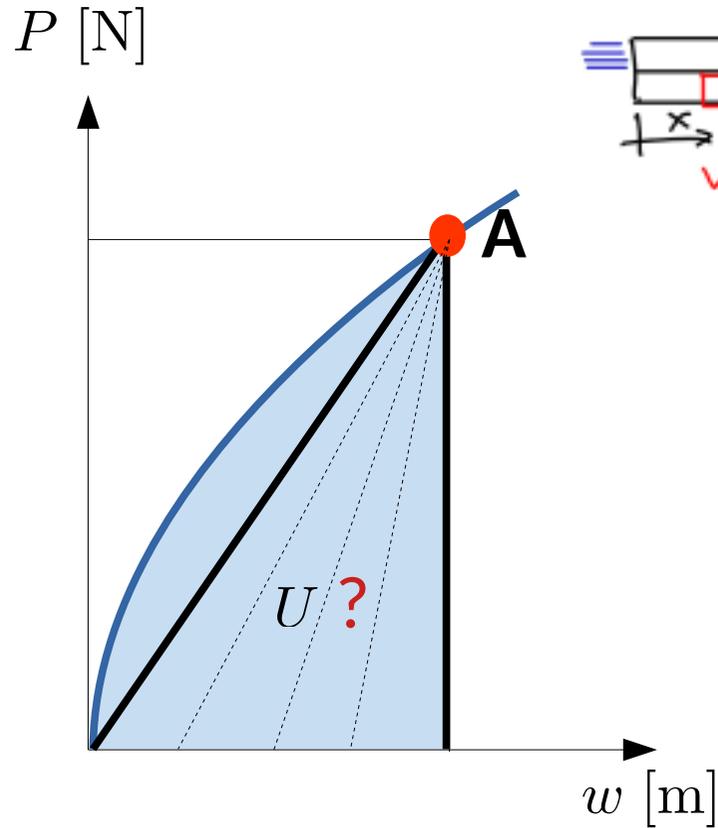
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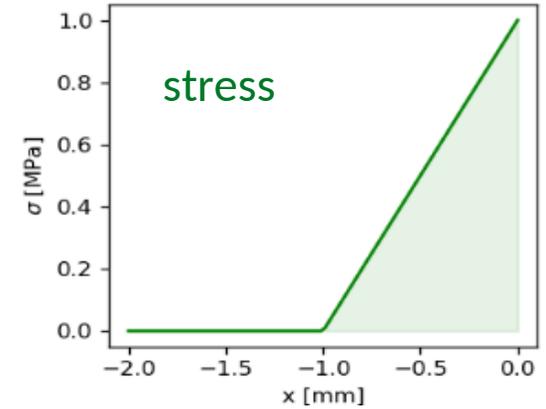
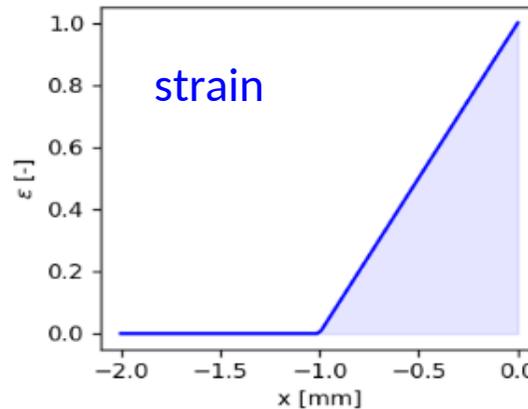
Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$U(w) = \int_{\Omega} E_f \varepsilon_f^2(x) dx$$



[see Tour 2]

$$W = \int_0^w P(w) dw$$

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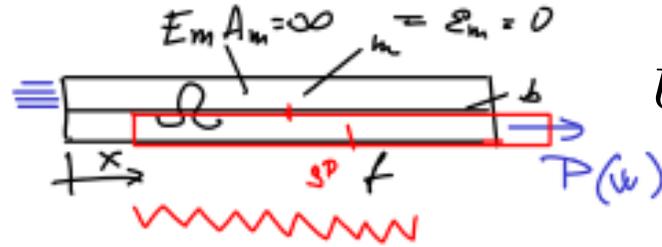
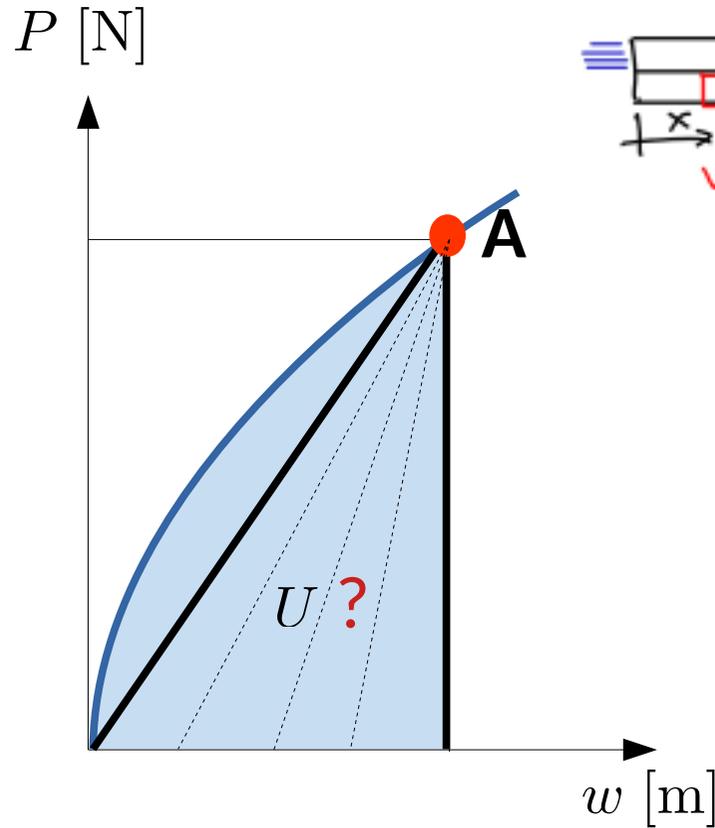
$$G = W - U$$

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Dissipated energy – pull-out from rigid matrix

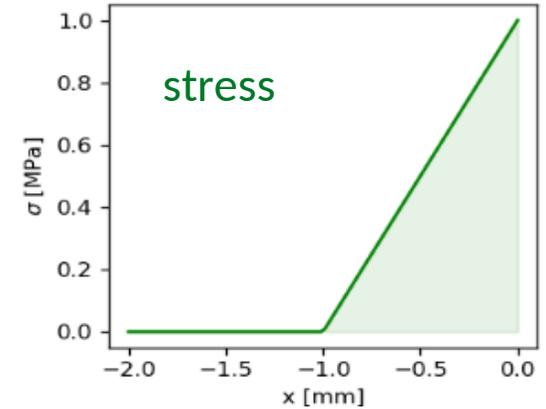
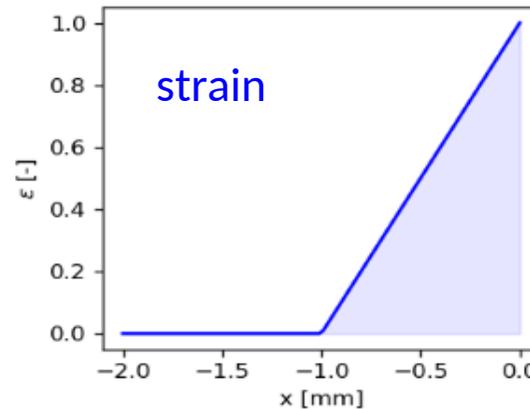
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$$U(w) = \int_{\Omega} E_f \varepsilon_f^2(x) dx$$

$$\varepsilon_f(w, x) = \frac{1}{E_f A_f} (\tau p x + \sqrt{E_f A_f \tau p w})$$



$$W = \int_0^w P(w) dw$$

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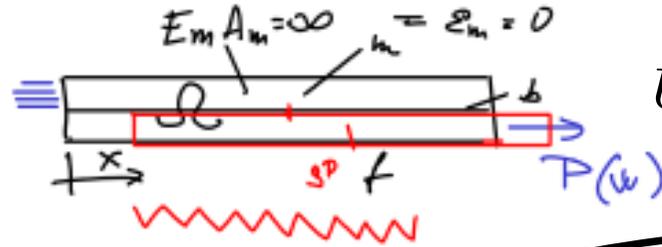
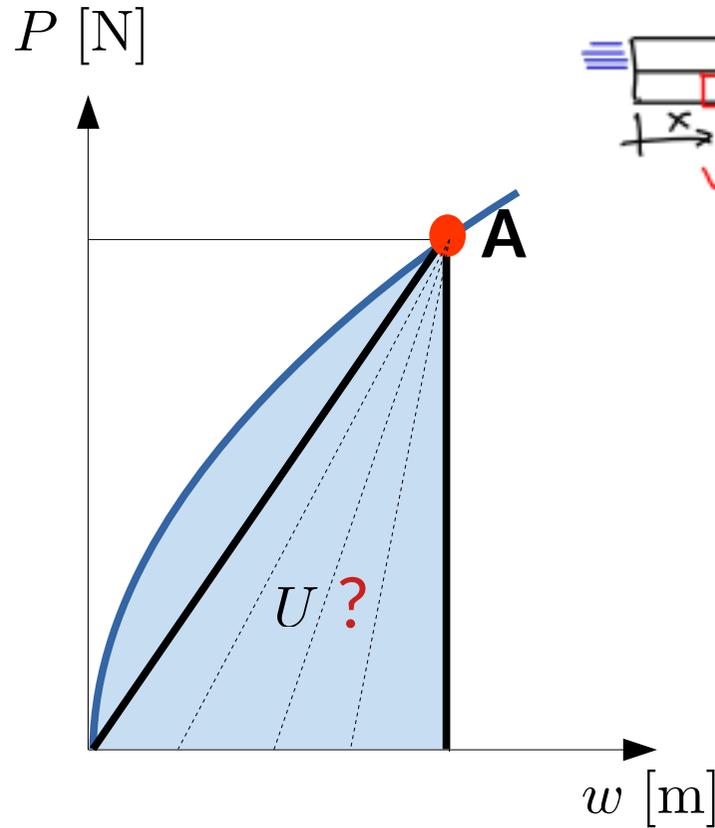
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Dissipated energy – pull-out from rigid matrix

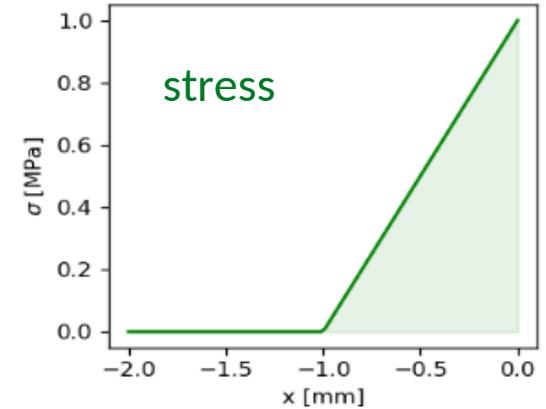
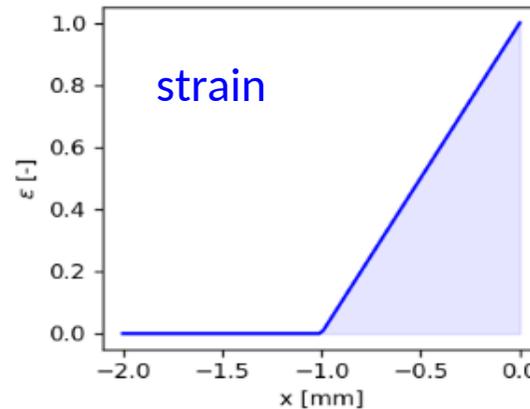
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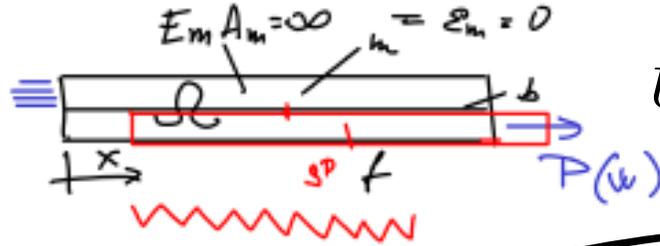
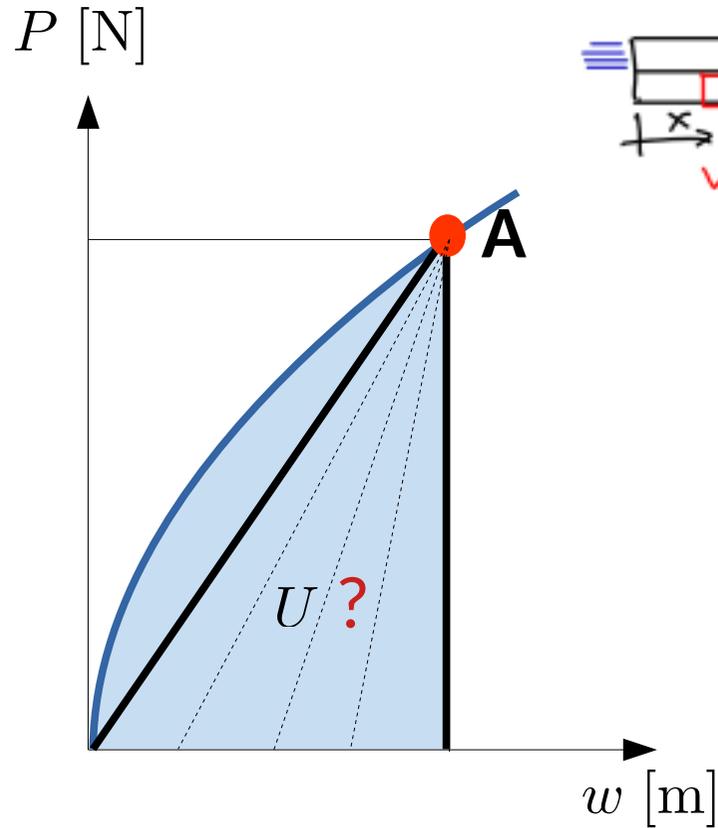
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Dissipated energy – pull-out from rigid matrix

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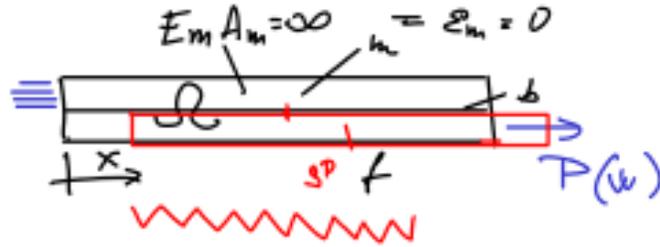
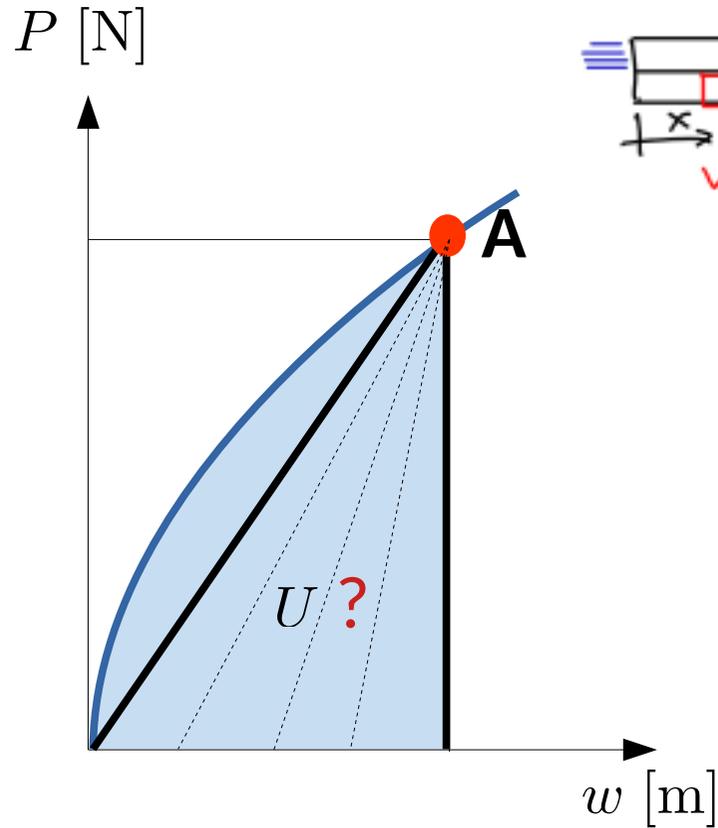
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Dissipated energy – pull-out from rigid matrix

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$$G = W - U$$

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Dissipated energy – pull-out from rigid matrix

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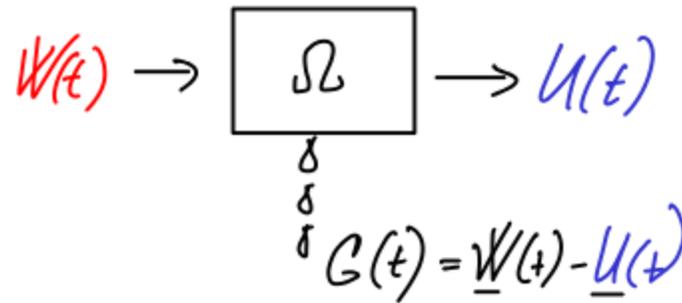
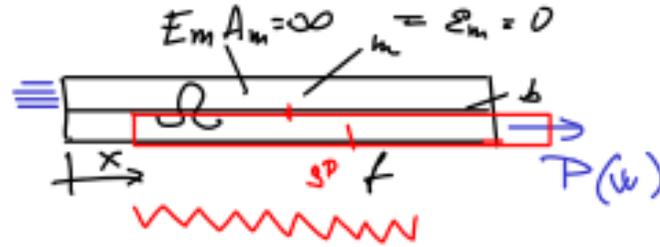
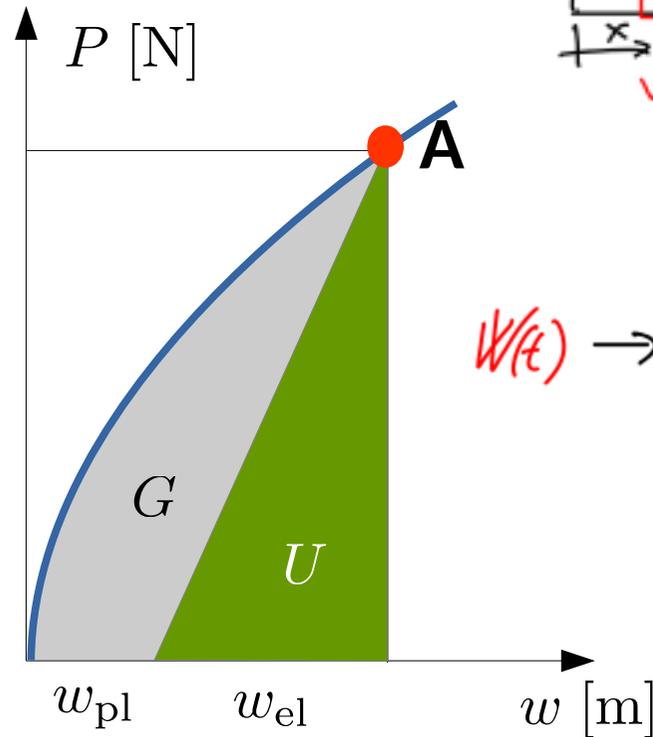
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$$G = \frac{\sqrt{2}}{3} \cdot \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

$$\Rightarrow G = U$$

DISSIPATED = STORED?



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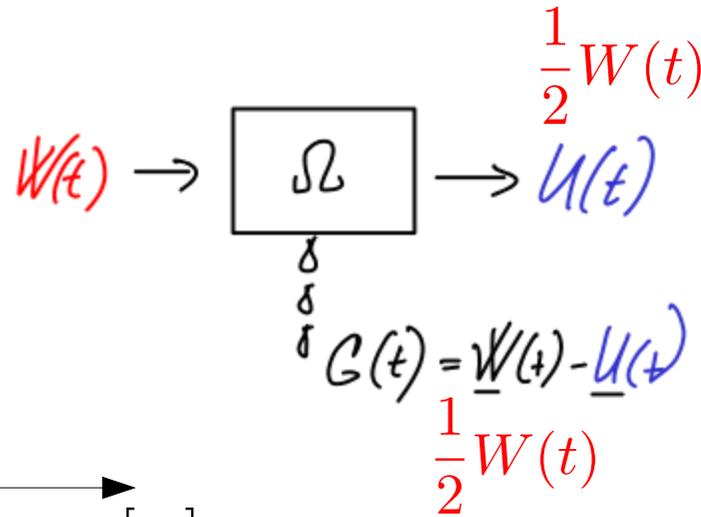
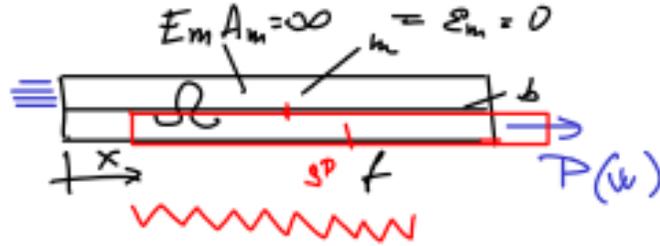
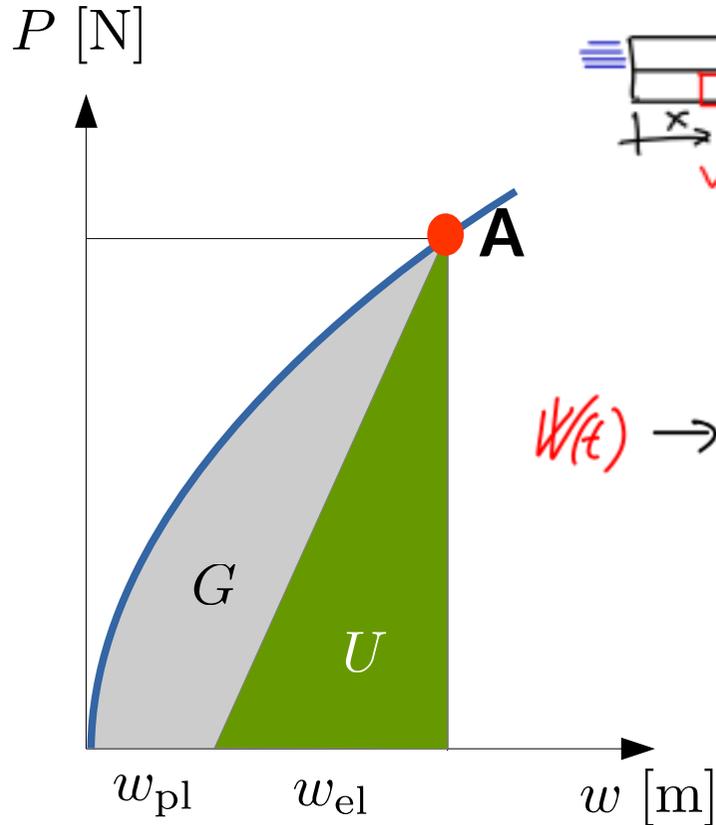
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Dissipated energy – pull-out from rigid matrix

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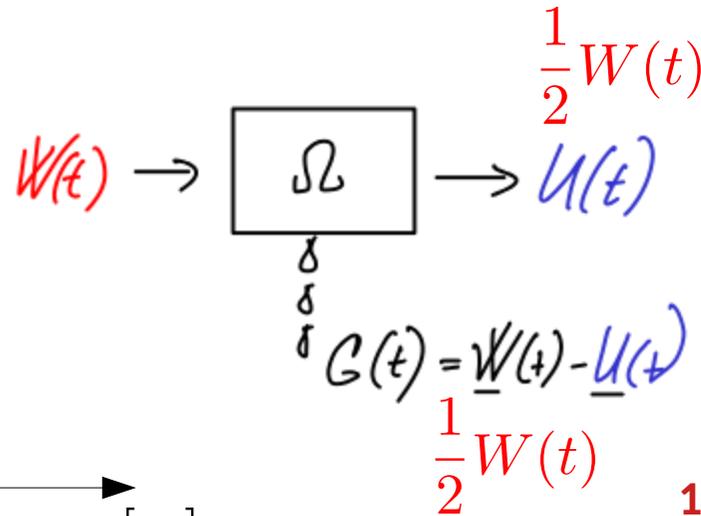
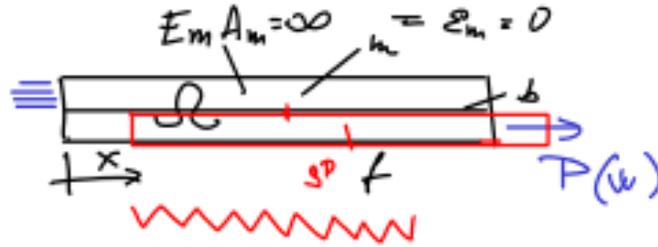
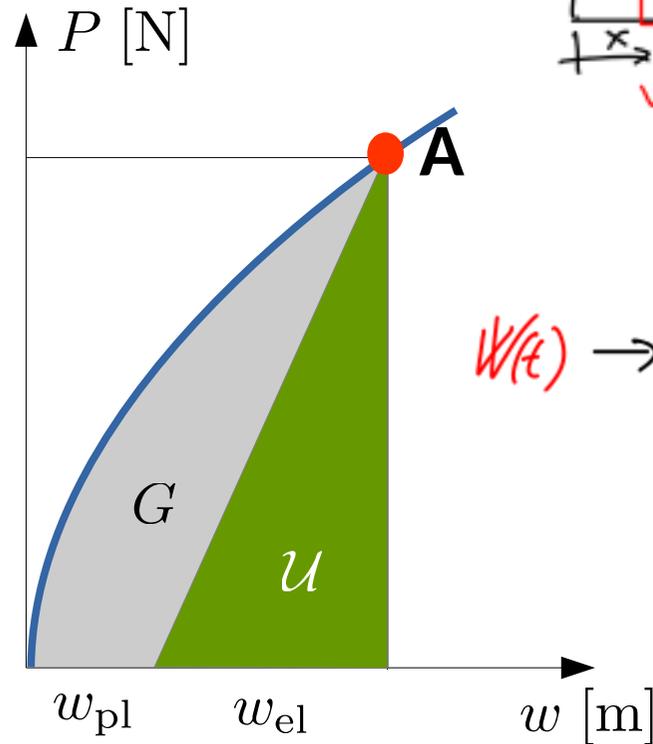
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$$\Rightarrow G = U$$



1. How much slip remains after unloading?

2. Dissipation and storage processes spatially separable?

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

$$U_\pi = \frac{P^2}{2K_0}$$

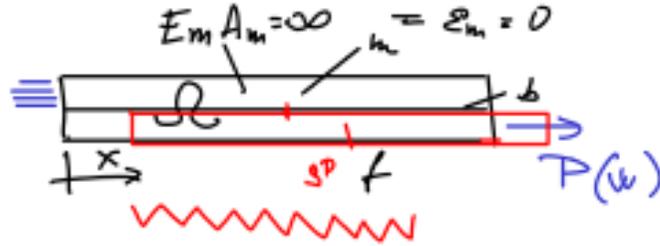
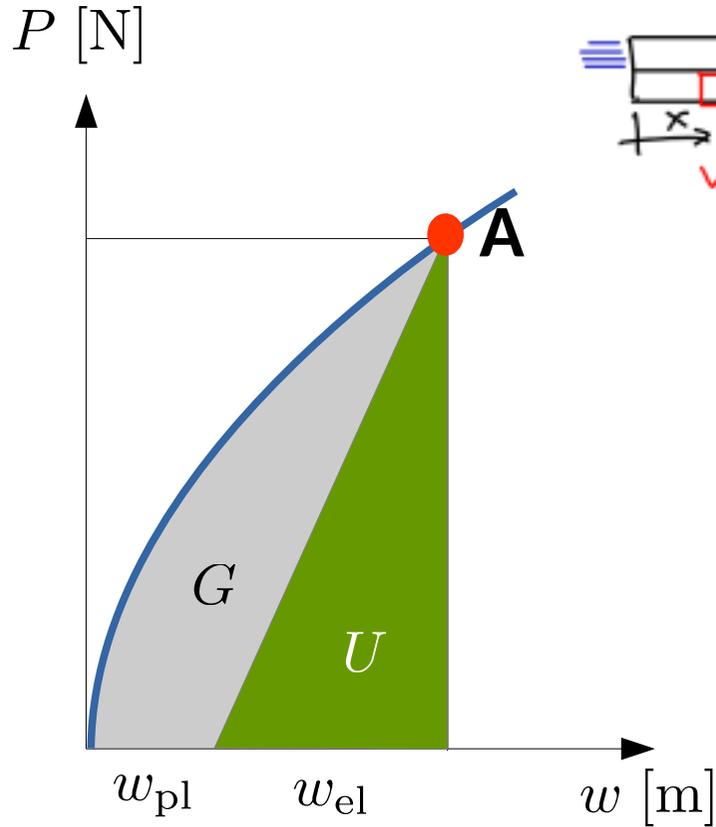
$$G = W - U$$

$$U = \int_{\Omega_{el}} \sigma(x) \varepsilon(x) dx$$

Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

$$G = W - U = \int_0^w P(w) dw - U(w)$$



$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

$$U = \frac{\sqrt{2}}{3} \cdot \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

$$G = \frac{\sqrt{2}}{3} \cdot \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

$$\implies G = U$$

$$U = \frac{1}{2} P w_{el}$$

$$w_{el} = \frac{2U}{P}$$

1. How much slip remains after unloading?

$$W = \int_0^w P(w) dw$$

$$U_w = \frac{1}{2} P w$$

$$U_\pi = \frac{P^2}{2K_0}$$

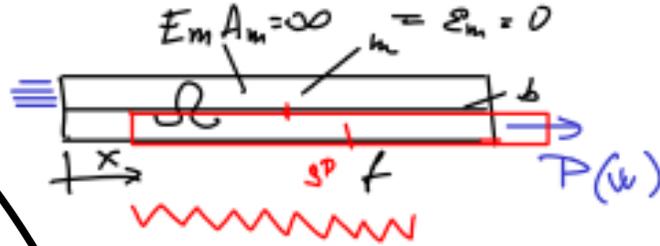
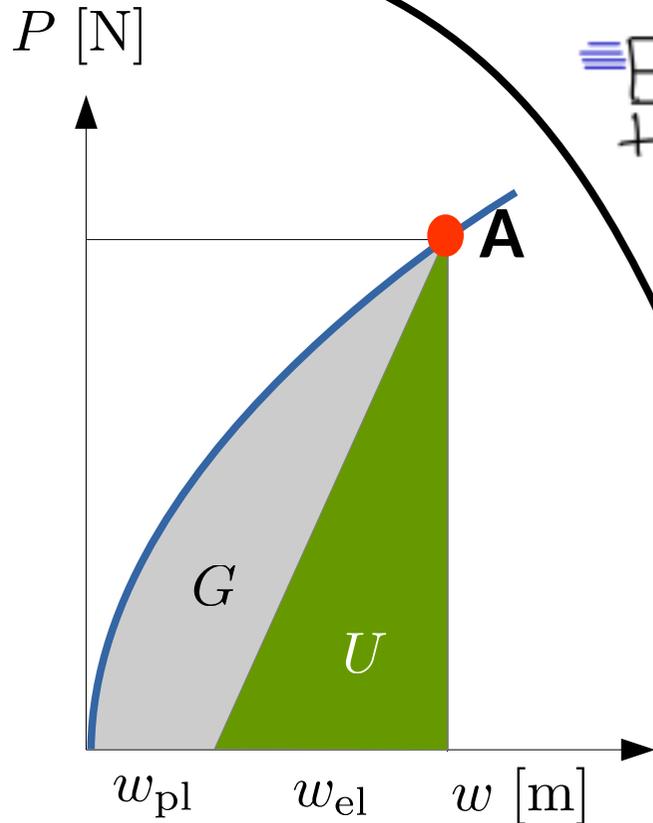
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Dissipated energy – pull-out from rigid matrix

$$P = \sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}} \sqrt{w}$$

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$$W = \frac{2\sqrt{2}}{3} \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

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$$\Rightarrow G = U$$

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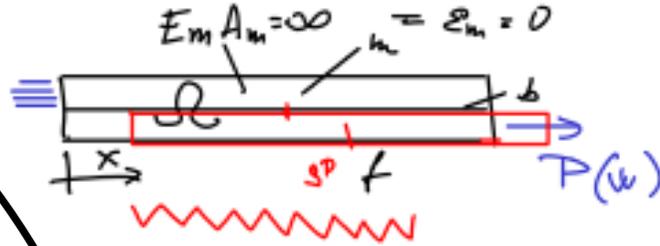
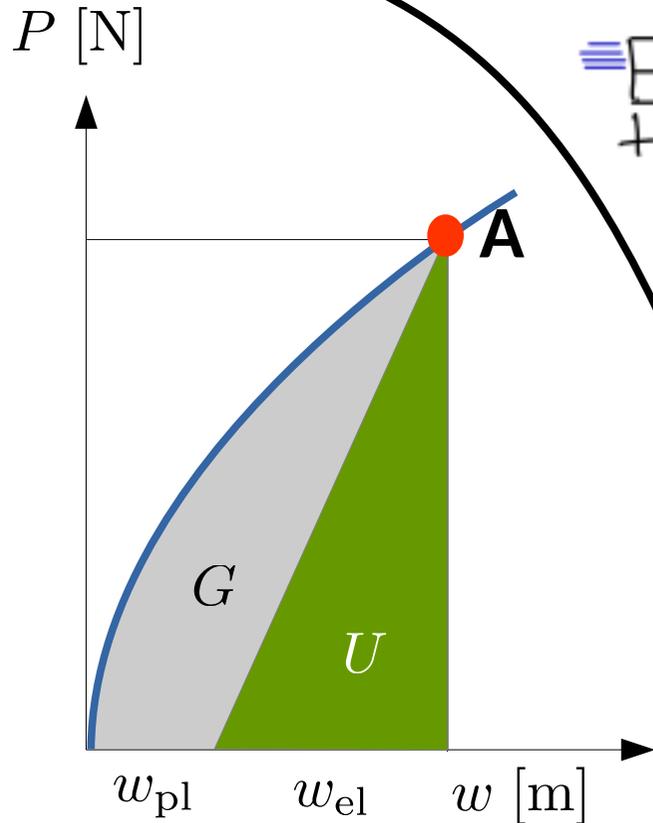
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Dissipated energy - pull-out from rigid matrix

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$$U = \frac{1}{2} P w_{el}$$

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$$\implies G = U$$

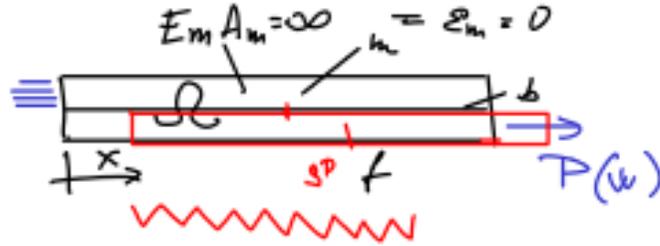
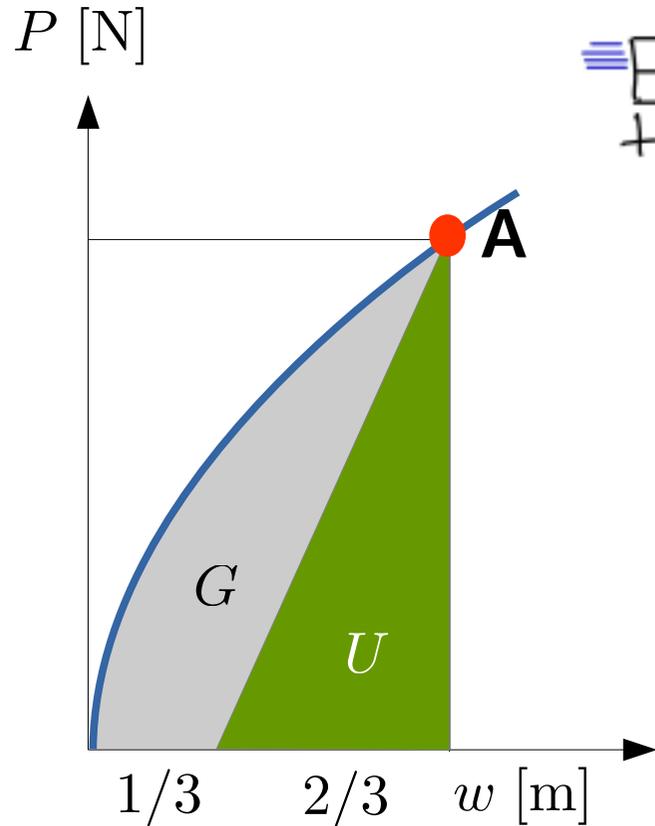
$$w_{el} = \frac{2\sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}}}{3\sqrt{2} \cdot \sqrt{E_f A_f p \bar{\tau}}} \cdot \frac{w^{\frac{3}{2}}}{w^{\frac{1}{2}}}$$

$$W = \int_0^w P(w) dw \quad U_w = \frac{1}{2} P w \quad U_\pi = \frac{P^2}{2K_0} \quad G = W - U \quad U = \int_{\Omega_{el}} \sigma(x) \varepsilon(x) dx$$

Dissipated energy – pull-out from rigid matrix

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$$U = \frac{1}{2} P w_{el}$$

$$G = \frac{\sqrt{2}}{3} \cdot \sqrt{E_f A_f p \bar{\tau}} \cdot w^{\frac{3}{2}}$$

$$w_{el} = \frac{2U}{P}$$

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$$W = \int_0^w P(w) dw$$

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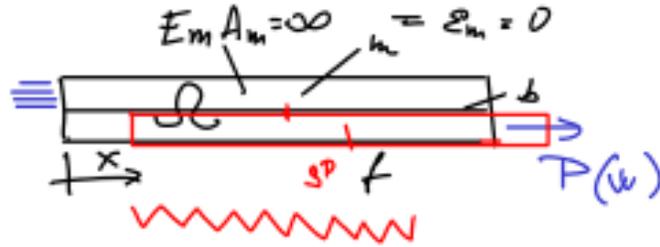
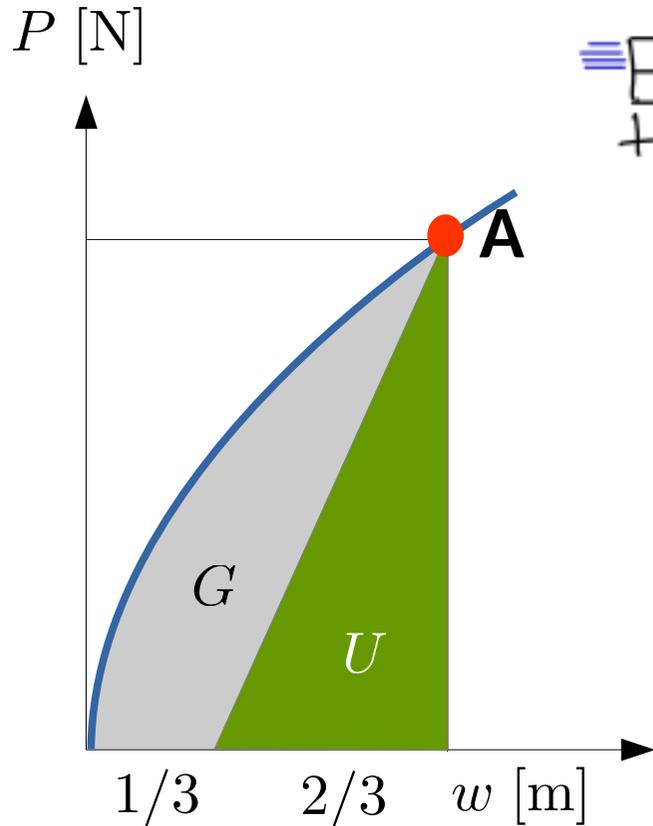
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Dissipated energy – pull-out from rigid matrix

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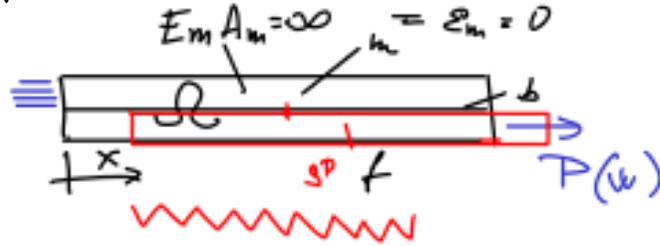
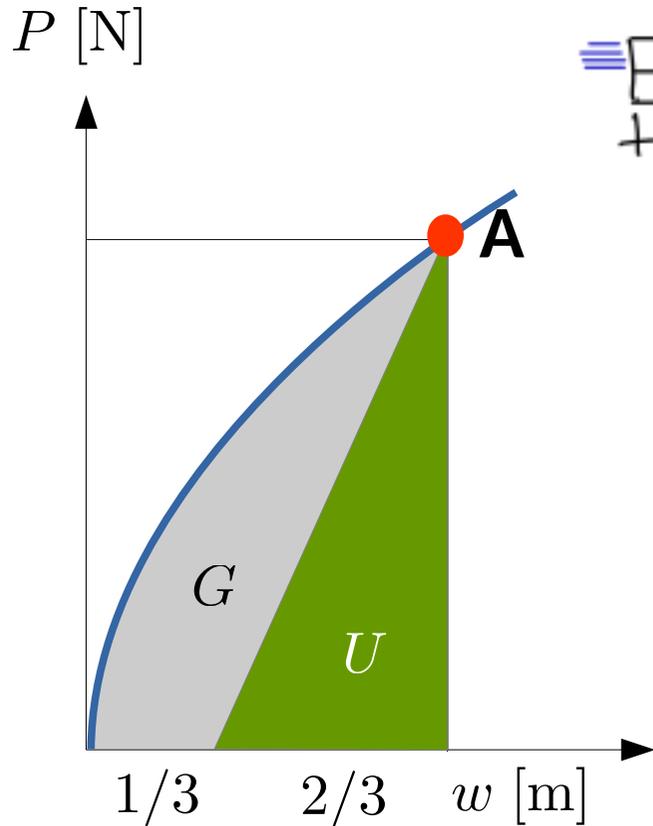
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How would you evaluate unloading stiffness?

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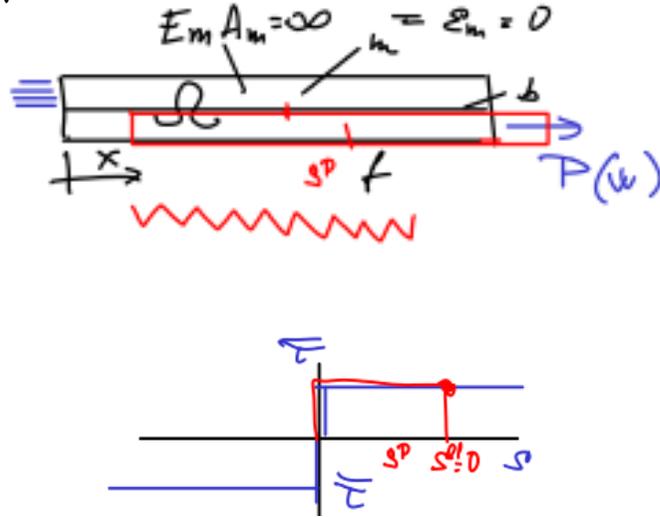
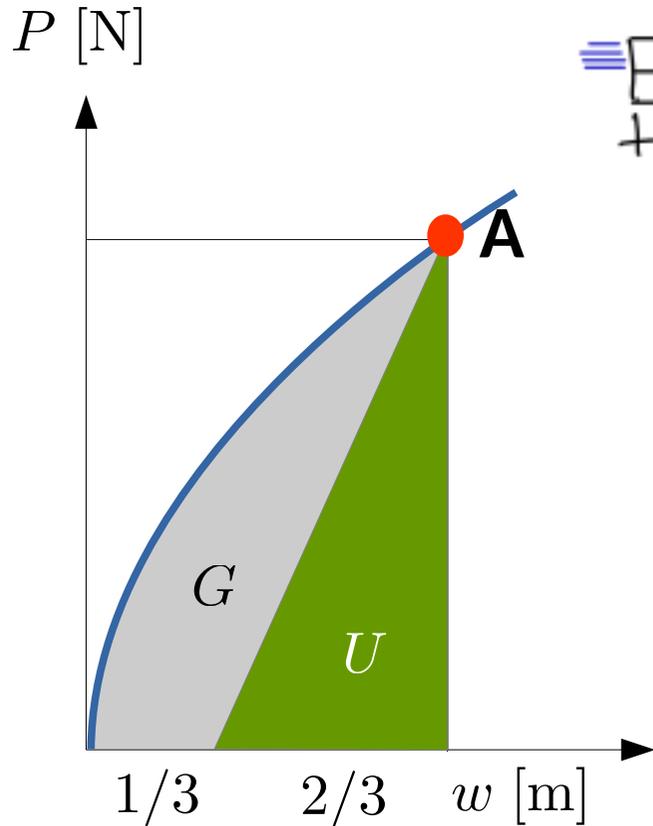
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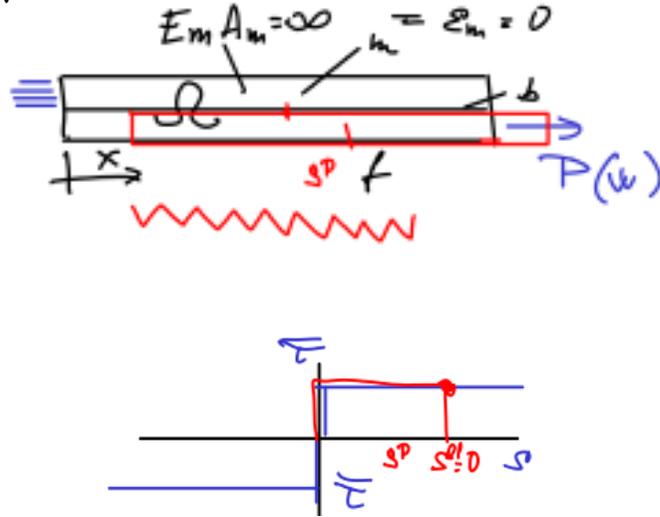
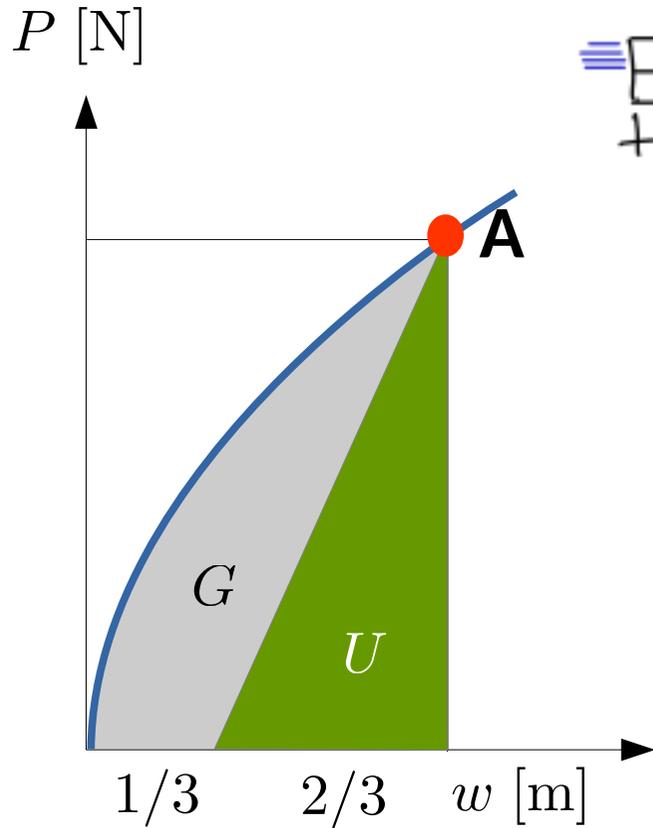
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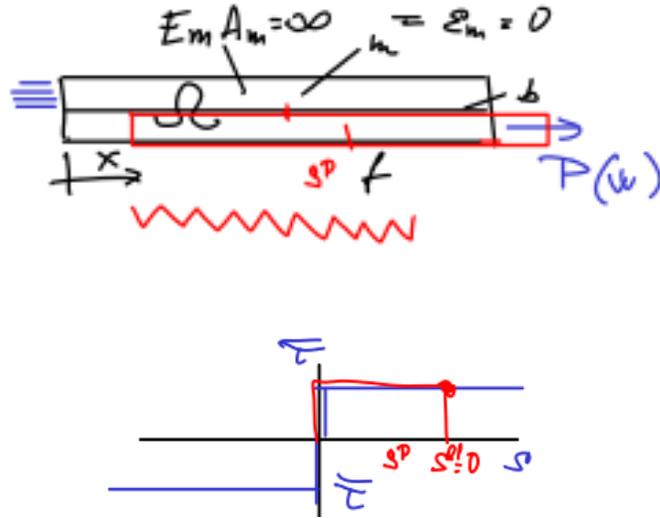
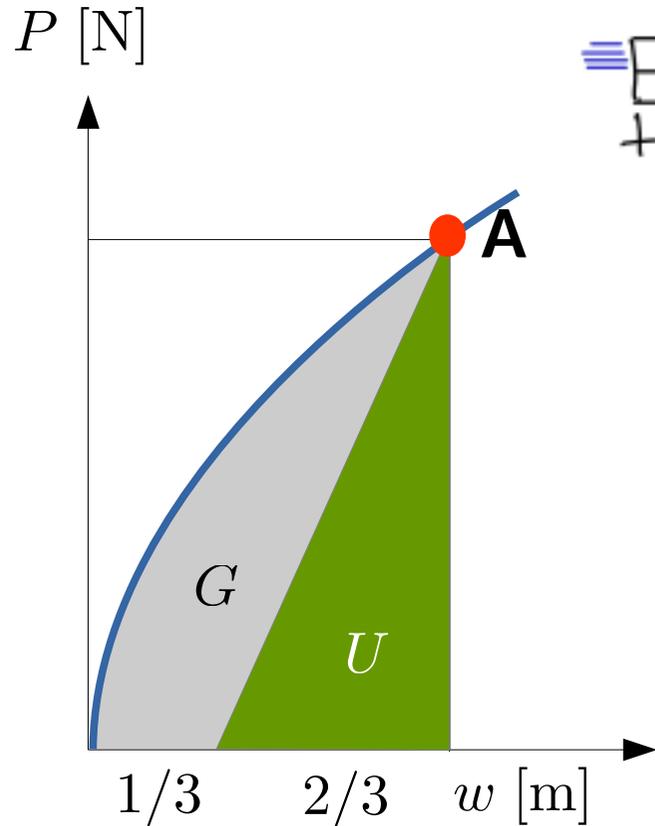
What? No damage, Perfect plasticity, but unloading somewhere in-between?

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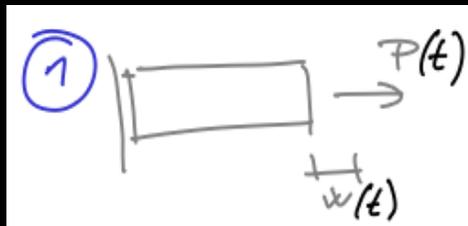
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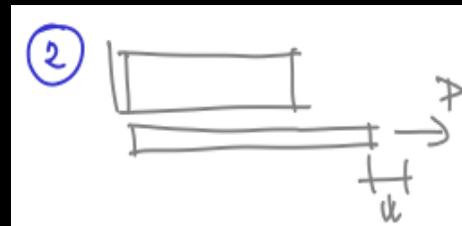
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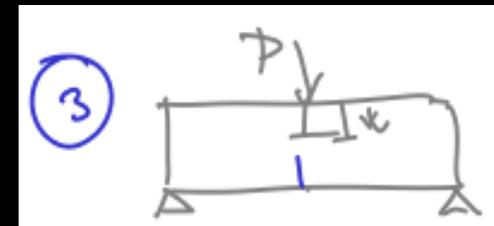
separation of domains with energy storage and dissipation



$$G = 0$$



$$G = U$$



$$G = ?$$

Dissipated energy → it tends to localize into a small material volume

Realize:

The example combined two energetic devices

one fully dissipative device → no energy storage (ideally plastic bond), and

one non-dissipative device → perfect energy storage (elastic bar)

Idea:

If it is possible to integrate the stored energy in all material points over the domain
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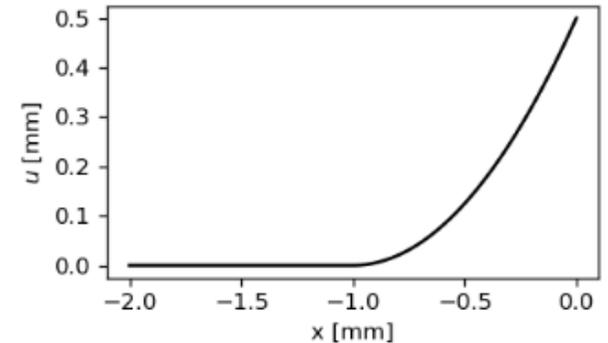
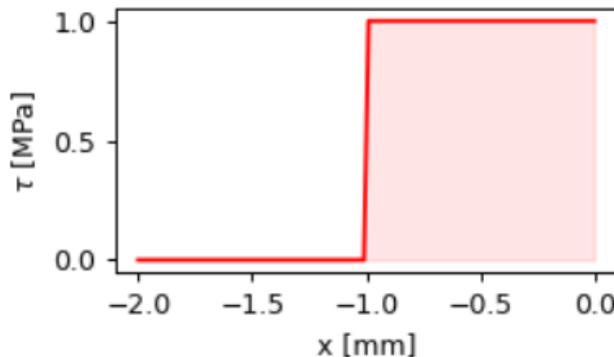
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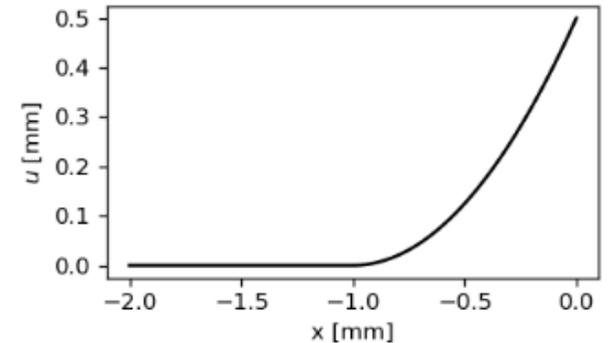
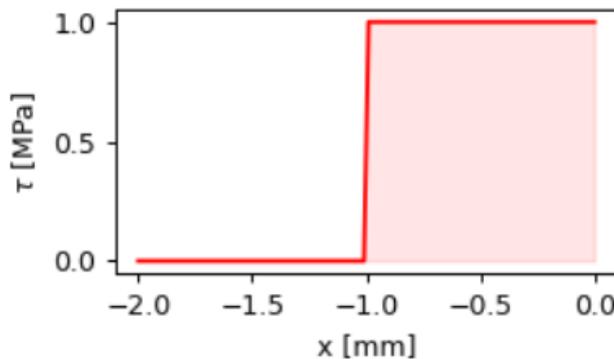
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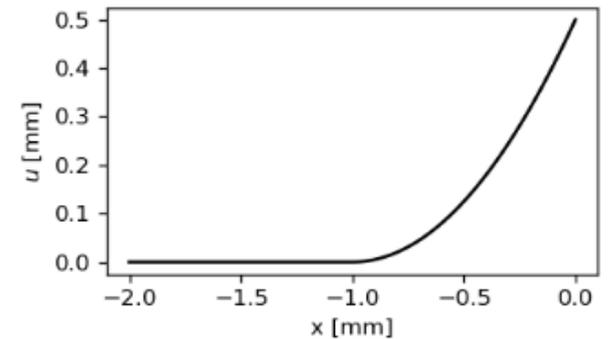
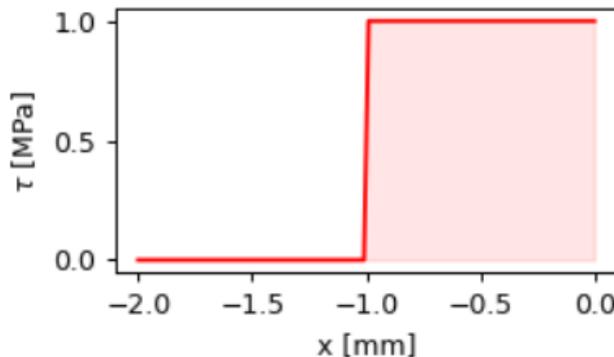
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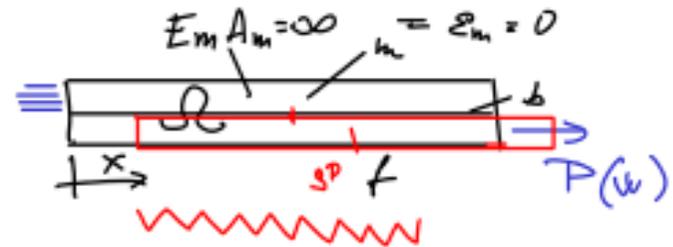
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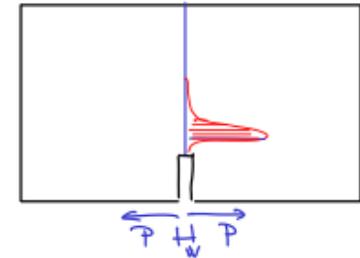
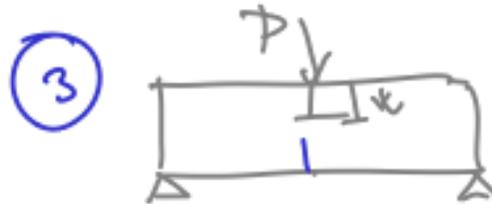
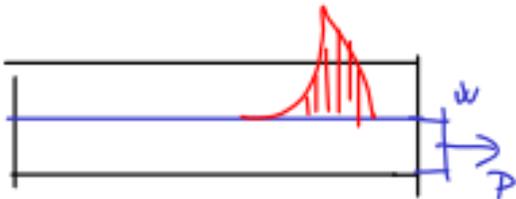
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This is really useful! We can evaluate dissipated energy locally!

If we know where the localization and crack propagation occurs, we can focus just onto this region and ignore the non-dissipative (elastic/unloading) rest of the domain

→ this is the fundamental concept behind methods describing **fracture**

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